

Controlling Human Heart Rate Response During Treadmill Exercise

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Hence, the existing linear models e.g. (Brodan, Hajek, & Kuhn, 1971) and (Cooper, Fletcher-Shaw, & Robertson, 1998) based on PID control may not be accurate.

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Model has been validated with human subjects. Unlike conventional linear models, it captures peripheral effects and is suitable for long duration exercise.

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is globally exponentially stable to zero, i.e., there are constants $c_i > 0$ so that $|\tilde{x}(t)| \leq c_1 e^{-c_2 t} |\tilde{x}(0)|$ for all trajectories of (1).

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Knowing x_{1r} allows us to solve for x_{2r} from (2b).

$$x_{2r}(t) = x_{2r}(0)e^{-a_3 t} + a_4 \int_0^t e^{a_3(\tau-t)} \frac{x_{1r}(\tau)}{1 + be^{-x_{1r}(\tau)}} d\tau. \quad (4)$$

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Then, we use (2a) to calculate $u_r(t) = \sqrt{J_{x_{1r}}(t)}$, where

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However, we need another condition to ensure trackability of x_r .

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$$\frac{a_1 a_3}{a_2 a_4} > P_\varepsilon \stackrel{\text{def}}{=} \max \left\{ \frac{1+\varepsilon}{\varepsilon}, \sup_{t \geq 0} \frac{1+b(1+\{1+\varepsilon\}x_{1r}(t))e^{-x_{1r}(t)}}{[1+be^{-\{1+\varepsilon\}x_{1r}(t)}][1+be^{-x_{1r}(t)}]} \right\} \quad (\text{SA})$$

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Cheng et al. use the Levenberg-Marquardt method to estimate the a_i 's.

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$$u_c(x, t) = \sqrt{\max \left\{ 0, u_r(t)^2 - \left(1 + \frac{R(\tilde{x}_1, t)}{P_\varepsilon} \right) \tilde{x}_2 \right\}},$$
$$\text{where } R(\tilde{x}_1, t) = \frac{1 + be^{-x_{1r}(t)} \left[1 + x_{1r}(t) \int_{-1}^0 e^{\tilde{x}_1 m} dm \right]}{(1 + be^{-(\tilde{x}_1 + x_{1r}(t))})(1 + be^{-x_{1r}(t)})}, \quad (6)$$

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Then $\dot{V} \leq -\sigma V$ along all trajectories of the closed loop system, where $\sigma = 2c_0 / \max\{k, 1\}$, $c_0 = \min\{-\lambda_{\max}, a_1, ka_3\}$, and $\lambda_{\max} < 0$ is the maximal eigenvalue of

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Observer Design

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$$u_c(x_1, \hat{x}_2, t) = \sqrt{\max \left\{ 0, u_r(t)^2 - \left(1 + \frac{R(\tilde{x}_1, t)}{P_\epsilon} \right) \hat{x}_2 \right\}}. \quad (7)$$

The estimate \hat{x}_2 of \tilde{x}_2 is from the observer

$$\begin{aligned} \dot{\hat{x}}_1 &= -a_1 \hat{x}_1 + a_2 \hat{x}_2 + k_1 \bar{x}_1 + a_2 [u_c^2(x_1, \hat{x}_2, t) - u_r(t)^2] \\ \dot{\hat{x}}_2 &= -a_3 \hat{x}_2 + a_4 R(\tilde{x}_1, t) \tilde{x}_1 + k_2 \bar{x}_1. \end{aligned} \quad (8)$$

Here $k_1 > 0$ and $k_2 > 0$ are tuning constants, and $\bar{x}_1 = \tilde{x}_1 - \hat{x}_1$.

Proposition. The (\tilde{x}, \bar{x}) dynamics in closed loop with (7) is globally exponentially stable to the origin.

Proof: Take $V^\sharp(\tilde{x}, \bar{x}) = V(\tilde{x}) + \bar{L}|\bar{x}|^2$ for a big enough $\bar{L} > 0$.

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 $a_5 = 8.32$ (Cheng et al., IEEE-TBE).

Simulations

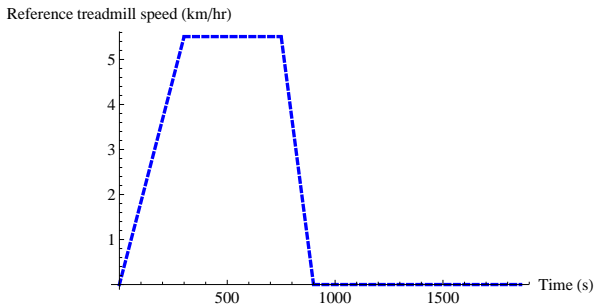
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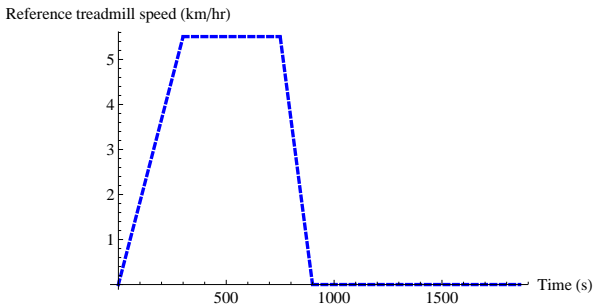
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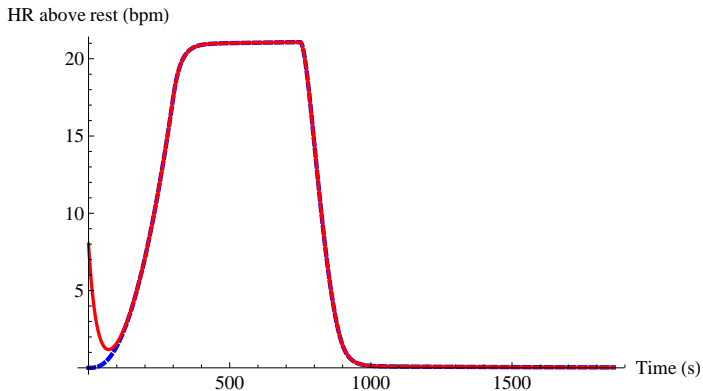
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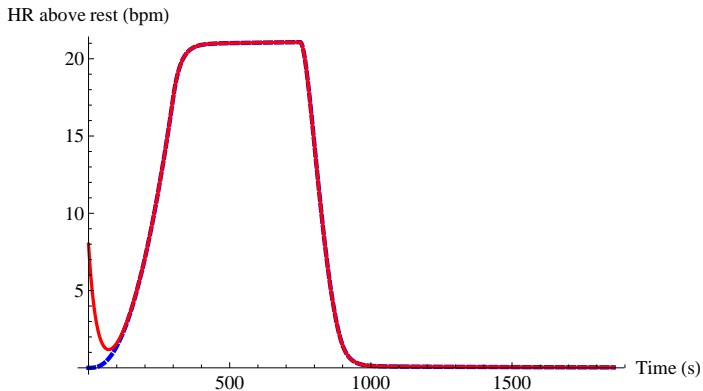
The resulting x_{1r} satisfies (SA) with $\varepsilon = 0.5$ so our results apply.

Tracking using State Feedback Control $u_c(x, t)$

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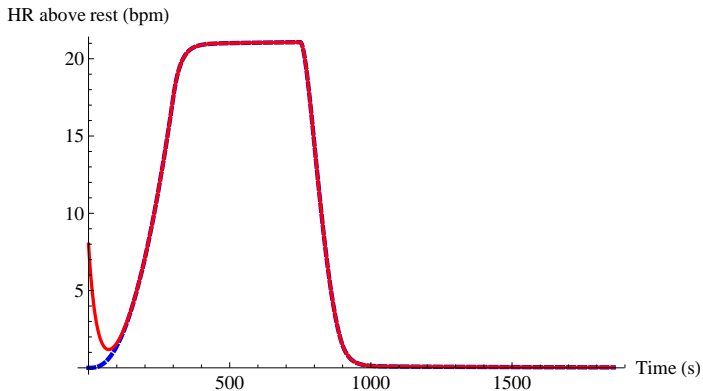


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x_{1r} (blue and dashed) and state x_1 (red and solid).

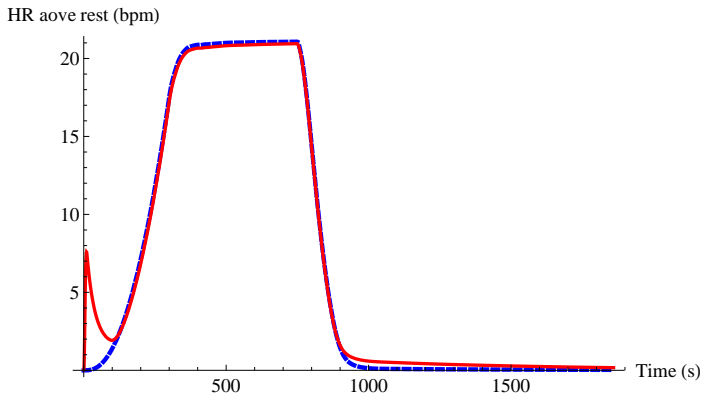
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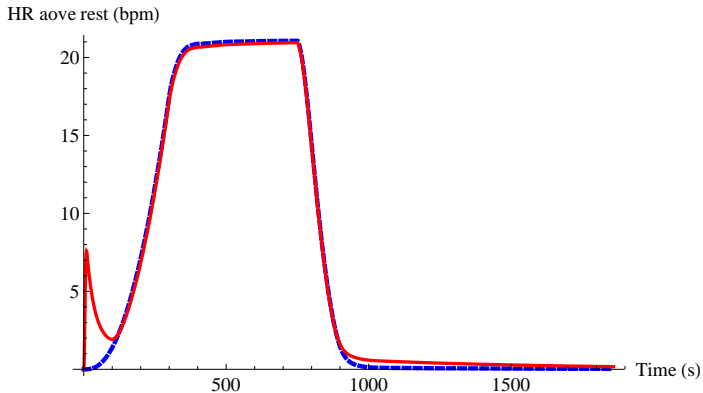
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Initial state: $x(0) = (2, 0)$.

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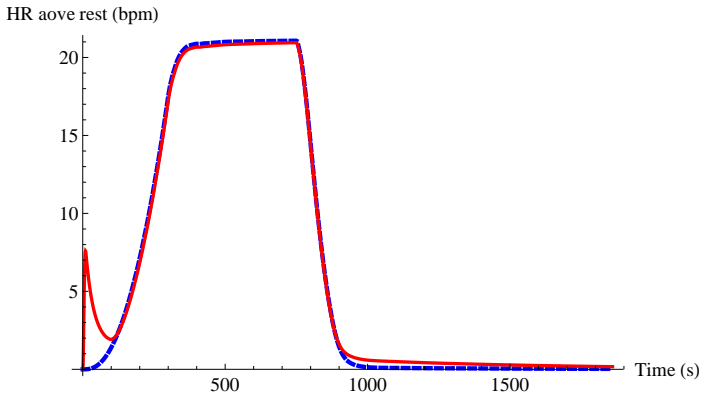


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Theorem: For each constant $\bar{\delta} > 0$, we can find constants $\bar{c}_i > 0$ depending on $\bar{\delta}$ so that along all trajectories of (9) for all measurable functions $\mathbf{d} : [0, \infty) \rightarrow [-\bar{\delta}, \bar{\delta}]$, we have

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This is input-to-state stability with exponential transient decay.

Ideas for Input-to-State Stability Proof

Step 1: Pick a positive definite quadratic function $W(\bar{x})$ such that

$$\dot{W} \leq -\frac{4a_2^2(1+8\bar{\delta}^2)}{c_0}|\bar{x}|^2 \quad (10)$$

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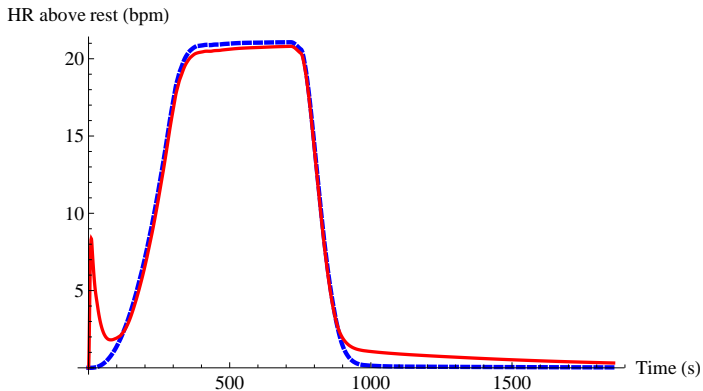
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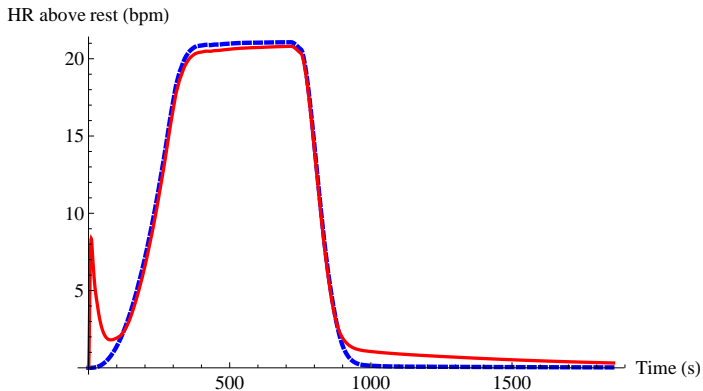
This means that $V^\#$ is an ISS Lyapunov function for (9) with disturbances \mathbf{d} bounded by $\bar{\delta}$ in the sup norm.

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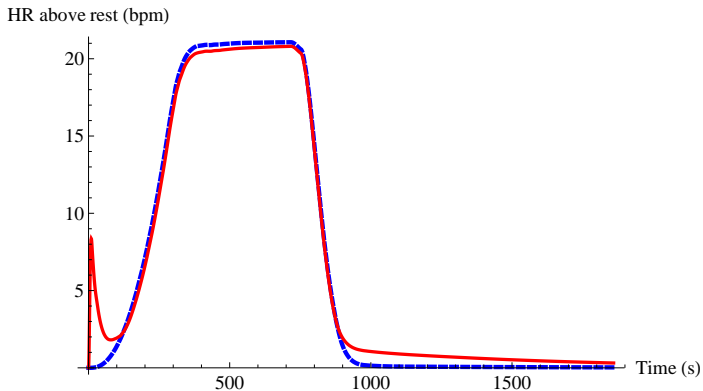


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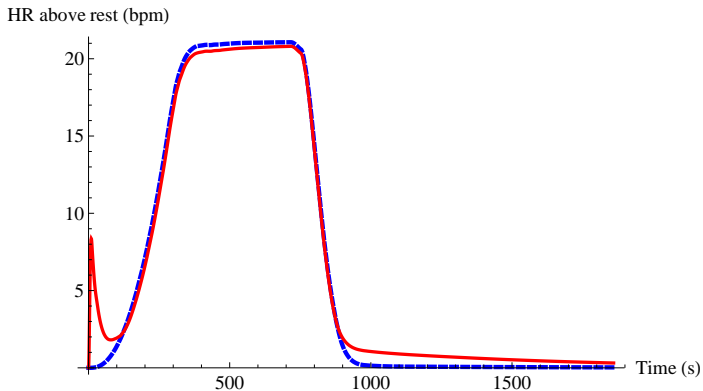
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- ▶ For complete proofs, see [FM, MM, and MdQ, "Tracking control and robustness analysis for a nonlinear model of human heart rate during exercise," *Automatica*, accepted.]