

Tracking Control for Neuromuscular Electrical Stimulation

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Our new **control** only needs sampled observations, allows any **delay**, and tracks position and velocity under a state constraint.

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$$Y'(t) = \mathcal{G}(t, Y_t, \delta(t)), \quad Y(t) \in \mathcal{Y}, \quad (2)$$

where $\mathcal{G}(t, Y_t, d) = \mathcal{F}(t, Y(t), \mathbf{u}(t, Y(t - \tau)), d)$.

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Typically we construct \mathbf{u} such that all trajectories of (2) for all possible choices of δ satisfy some control objective.

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Find γ_i 's by building certain LKFs for $Y'(t) = \mathcal{G}(t, Y_t, 0)$.

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- E_3 Step E_2 is often done by converting V into an ISS-LKF $V^\#$.

NMES on Leg Extension Machine

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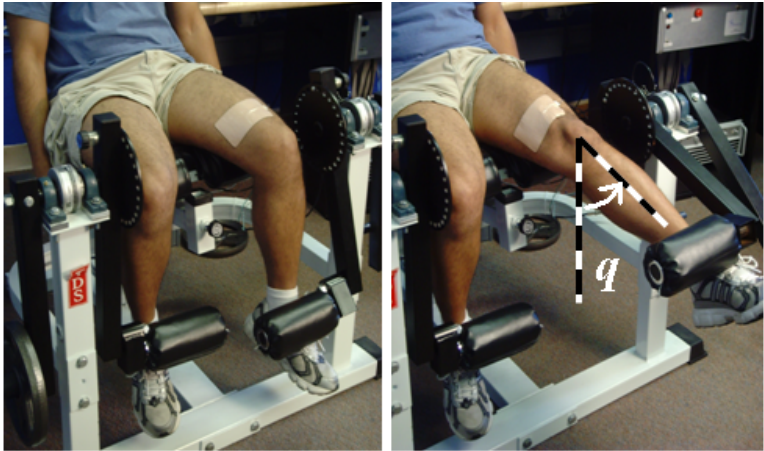
Leg extension machine at Warren Dixon's NCR Lab at U of FL

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Knee Joint Dynamics (Sharma et al, 2009)

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$M_e(q) = k_1 q e^{-k_2 q} + k_3 \tan(q)$: **elastic effects** due to joint stiffness with constants $k_i > 0$. We introduce the tan term to accommodate our state constraint $q \in (-\pi/2, \pi/2)$.

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$M_g(q) = \mathcal{M}gl \sin(q)$: **gravitational component**. \mathcal{M} = mass of shank and foot, g = gravitational acceleration, l = distance between knee-joint and lumped center of mass of shank-foot.

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$F = \xi(q, \dot{q})v(t - \tau)$: v = voltage across quadriceps.
 τ = latency between applying voltage and force production.

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$$\begin{aligned}
 & \overbrace{J\ddot{q}}^{M_I(\ddot{q})} + \overbrace{b_1\dot{q} + b_2 \tanh(b_3\dot{q})}^{M_V(\dot{q})} + \overbrace{k_1 q e^{-k_2 q} + k_3 \tan(q)}^{M_E(q)} \\
 & + \underbrace{\mathcal{M}gl \sin(q)}_{M_g(q)} = \mathcal{A}(q, \dot{q}) \mathcal{V}(t - \tau), \quad q \in \left(-\frac{\pi}{2}, \frac{\pi}{2}\right)
 \end{aligned} \tag{3}$$

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Our Requirements:

- $F : (-\pi/2, \pi/2) \rightarrow [0, \infty)$ is C^2 and $\lim_{q \rightarrow \pm\pi/2} F(q) = \infty$.
- $G : (-\pi/2, \pi/2) \times \mathbb{R} \rightarrow (0, \infty)$ is C^1 and bounded.
- $H : \mathbb{R} \rightarrow \mathbb{R}$ is C^1 and $\inf_{x \in \mathbb{R}} xH(x) \geq 0$.

Tracking Problem

$$\ddot{q}(t) = -\frac{dF}{dq}(q(t)) - H(\dot{q}(t)) + G(q(t), \dot{q}(t))v(t - \tau) \quad (4)$$

$$\begin{aligned} F(q) &= \frac{k_1 \exp(-k_2 q)}{Jk_2^2} (\exp(k_2 q) - 1 - k_2 q) \\ &\quad + \frac{mgl}{J} (1 - \cos(q)) + \frac{k_3}{J} \ln \left(\frac{1}{\cos(q)} \right), \\ G(q, \dot{q}) &= \frac{1}{J} \mathcal{A}(q, \dot{q}), \text{ and} \\ H(\dot{q}) &= \frac{b_2}{J} \tanh(b_3 \dot{q}) + \frac{b_1}{J} \dot{q}. \end{aligned} \quad (5)$$

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$$\begin{aligned} F(q) &= \frac{k_1 \exp(-k_2 q)}{Jk_2^2} (\exp(k_2 q) - 1 - k_2 q) \\ &\quad + \frac{mgl}{J} (1 - \cos(q)) + \frac{k_3}{J} \ln \left(\frac{1}{\cos(q)} \right), \\ G(q, \dot{q}) &= \frac{1}{J} \mathcal{A}(q, \dot{q}), \text{ and} \\ H(\dot{q}) &= \frac{b_2}{J} \tanh(b_3 \dot{q}) + \frac{b_1}{J} \dot{q}. \end{aligned} \quad (5)$$

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We want $(q - q_d, \dot{q} - \dot{q}_d) \rightarrow 0$ in a UGAS exponential way.

Voltage Controller

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Error variables:

$$x_1 = \tan(q) - \tan(q_d) \text{ and } x_2 = \frac{\dot{q}}{\cos^2(q)} - \frac{\dot{q}_d}{\cos^2(q_d)}$$

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Three parts of the control scheme, assuming $t_0 = 0$:

A numerical prediction $\xi(T_i) = z_{N_i}$ of the error variables at time $T_i + \tau$ using $(q(T_i), \dot{q}(T_i)) \in (-\pi/2, \pi/2) \times \mathbb{R}$.

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Applying the predictor feedback $v(t)$, i.e., the nominal control with the state variables replaced by their predicted values.

Voltage Controller

$$v(t) = \frac{g_2(\zeta_d(t+\tau))v_d(t) - g_1(\zeta_d(t+\tau) + \xi(t)) + g_1(\zeta_d(t+\tau)) - (1 + \mu^2)\xi_1(t) - 2\mu\xi_2(t)}{g_2(\zeta_d(t+\tau) + \xi(t))}$$

for all $t \in [T_i, T_{i+1})$ and each i

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$$g_1(x) = -(1 + x_1^2) \frac{dF}{dq}(\tan^{-1}(x_1)) + \frac{2x_1x_2^2}{1+x_1^2} - (1 + x_1^2)H\left(\frac{x_2}{1+x_1^2}\right),$$

$$g_2(x) = (1 + x_1^2)G\left(\tan^{-1}(x_1), \frac{x_2}{1+x_1^2}\right),$$

$$\zeta_d(t) = (\zeta_{1,d}(t), \zeta_{2,d}(t)) = \left(\tan(q_d(t)), \frac{\dot{q}_d(t)}{\cos^2(q_d(t))}\right),$$

$$\xi_1(t) = e^{-\mu(t-T_i)} \{ (\xi_2(T_i) + \mu\xi_1(T_i)) \sin(t - T_i) + \xi_1(T_i) \cos(t - T_i) \},$$

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and $\xi(T_i) = z_{N_i}$.

Voltage Controller

$$v(t) = \frac{g_2(\zeta_d(t+\tau))v_d(t) - g_1(\zeta_d(t+\tau) + \xi(t)) + g_1(\zeta_d(t+\tau)) - (1+\mu^2)\xi_1(t) - 2\mu\xi_2(t)}{g_2(\zeta_d(t+\tau) + \xi(t))}$$

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and $\xi(T_i) = z_{N_i}$. The time-varying Euler iterations $\{z_k\}$ at each time T_i use measurements $(q(T_i), \dot{q}(T_i))$.

Voltage Potential Controller (continued)

Euler iterations used for **control**:

$z_{k+1} = \Omega(T_i + kh_i, h_i, z_k; \mathbf{v})$ for $k = 0, \dots, N_i - 1$, where

$$z_0 = \begin{pmatrix} \tan(q(T_i)) - \tan(q_d(T_i)) \\ \frac{\dot{q}(T_i)}{\cos^2(q(T_i))} - \frac{\dot{q}_d(T_i)}{\cos^2(q_d(T_i))} \end{pmatrix}, \quad h_i = \frac{\tau}{N_i},$$

and $\Omega : [0, +\infty)^2 \times \mathbb{R}^2 \rightarrow \mathbb{R}^2$ is defined by

$$\Omega(T, h, x; \mathbf{v}) = \begin{bmatrix} \Omega_1(T, h, x; \mathbf{v}) \\ \Omega_2(T, h, x; \mathbf{v}) \end{bmatrix} \quad (8)$$

and the formulas

$$\Omega_1(T, h, x; \mathbf{v}) = x_1 + hx_2 \quad \text{and}$$

$$\begin{aligned} \Omega_2(T, h, x; \mathbf{v}) = & x_2 + \zeta_{2,d}(T) + \int_T^{T+h} \mathbf{g}_1(\zeta_d(s) + x) ds \\ & + \int_T^{T+h} \mathbf{g}_2(\zeta_d(s) + x) \mathbf{v}(s - \tau) ds - \zeta_{2,d}(T+h). \end{aligned}$$

NMES Theorem (IK, MM, MK, Ruzhou, IJRNC)

For each pair $(\tau, r) \in (0, \infty)^2$, there exist a locally bounded function N , a constant $\omega \in (0, \mu/2)$ and a locally Lipschitz function C satisfying $C(0) = 0$ such that: For all sample times $\{T_i\}$ in $[0, \infty)$ such that $\sup_{i \geq 0} (T_{i+1} - T_i) \leq r$ and each initial condition, the solution $(q(t), \dot{q}(t), \mathbf{v}(t))$ with

$$N_i = N \left(\left| \left(\tan(q(T_i)), \frac{\dot{q}(T_i)}{\cos^2(q(T_i))} \right) - \zeta_d(T_i) \right| + \|\mathbf{v} - \mathbf{v}_d\|_{[T_i - \tau, T_i]} \right) \quad (9)$$

satisfies

$$\begin{aligned} & |q(t) - q_d(t)| + |\dot{q}(t) - \dot{q}_d(t)| + \|\mathbf{v} - \mathbf{v}_d\|_{[t - \tau, t]} \\ & \leq e^{-\omega t} C \left(\frac{|q(0) - q_d(0)| + |\dot{q}(0) - \dot{q}_d(0)|}{\cos^2(q(0))} + \|\mathbf{v}_0 - \mathbf{v}_d\|_{[-\tau, 0]} \right) \end{aligned}$$

for all $t \geq 0$.

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$$\tau = 0.07\text{s}, \quad \mathcal{A}(q, \dot{q}) = \bar{a}e^{-2q^2} \sin(q) + \bar{b}$$

$$\begin{aligned} J &= 0.39 \text{ kg-m}^2/\text{rad}, \quad b_1 = 0.6 \text{ kg-m}^2/(\text{rad-s}), \quad \bar{a} = 0.058, \\ b_2 &= 0.1 \text{ kg-m}^2/(\text{rad-s}), \quad b_3 = 50 \text{ s/rad}, \quad \bar{b} = 0.0284, \\ k_1 &= 7.9 \text{ kg-m}^2/(\text{rad-s}^2), \quad k_2 = 1.681/\text{rad}, \\ k_3 &= 1.17 \text{ kg-m}^2/(\text{rad-s}^2), \quad \mathcal{M} = 4.38 \text{ kg}, \quad l = 0.248 \text{ m}. \end{aligned} \quad (11)$$

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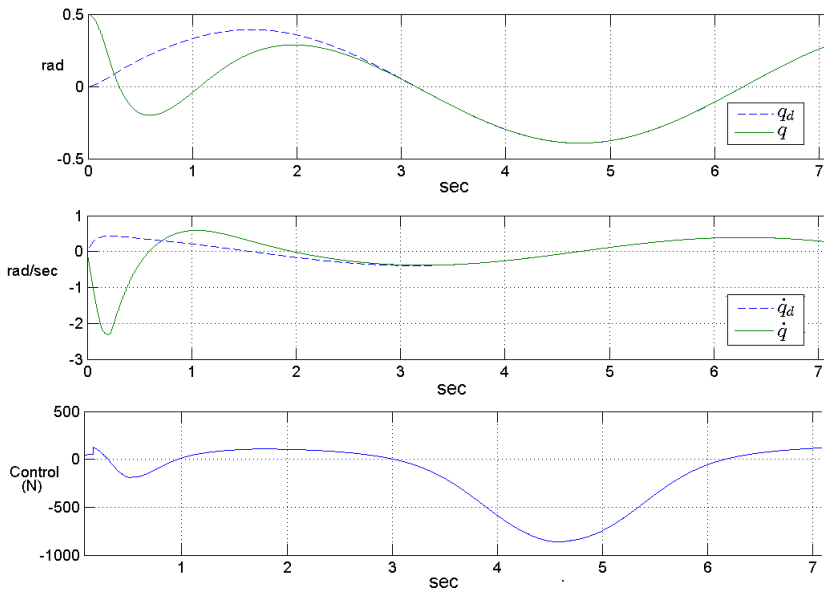
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$$q(0) = 0.5 \text{ rad}, \quad \dot{q}(0) = 0 \text{ rad/s}, \quad \mathbf{v}(t) = 0 \text{ on } [-0.07, 0), \\ N_i = N = 10, \text{ and } T_{i+1} - T_i = 0.014\text{s}, \text{ and } \mu = 2.$$

MATLAB Simulation



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In future work, we hope to apply input-to-state stability to better understand the effects of uncertainties under state constraints.