

Systems and Control: An Introduction and a Marine Robotics Application

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Sponsor: NSF Energy, Power, and Adaptive Systems
Joint with Fumin Zhang's Team at Georgia Tech

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Problem: Given a desired reference trajectory Y_r , specify u and a dynamics for an estimate $\hat{\Gamma}$ of Γ such that the augmented error $\mathcal{E}(t) = (Y(t) - Y_r(t), \Gamma - \hat{\Gamma}(t))$ satisfies **ISS** with respect to δ .

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When $\tau = 0$, a system is **ISS** iff it has an **ISS** LF (Sontag-Wang).

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For many systems, we design controls u that ensure ISS under the delays τ and uncertainties δ that prevail in engineering.

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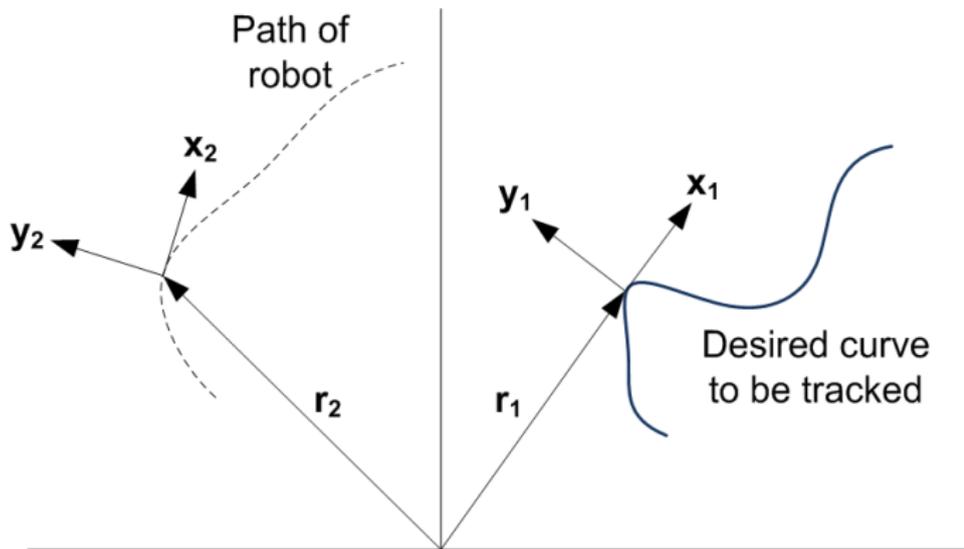
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Motivation: Pollutants from Deepwater Horizon oil spill.

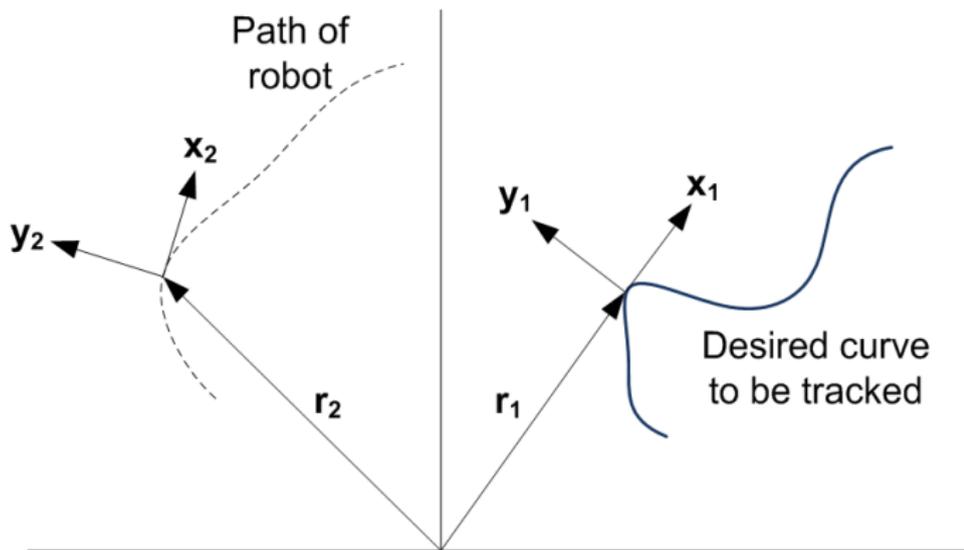
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$$\rho = |\mathbf{r}_2 - \mathbf{r}_1|, \phi = \text{angle between } \mathbf{x}_1 \text{ and } \mathbf{x}_2, \cos(\phi) = \mathbf{x}_1 \cdot \mathbf{x}_2$$

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In the new variables ρ and $z = \sin(\phi)$, the system (Σ) becomes

$$\dot{\rho} = -z, \quad \dot{z} = \frac{\kappa(1-z^2)}{1+\kappa\rho} - u\sqrt{1-z^2} \quad (\Sigma_c)$$

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Proposition: There do not exist constants $K_1 > 0$ and $K_2 > 0$ such that $\mathcal{X}_c = (0, \infty) \times (-1, 1)$ is forward invariant for (3).

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Assumption 1: $h : (0, +\infty) \rightarrow [0, \infty)$ is C^1 , h' has only finitely many zeros, $\lim_{\rho \rightarrow 0^+} h(\rho) = \lim_{\rho \rightarrow \infty} h(\rho) = \infty$

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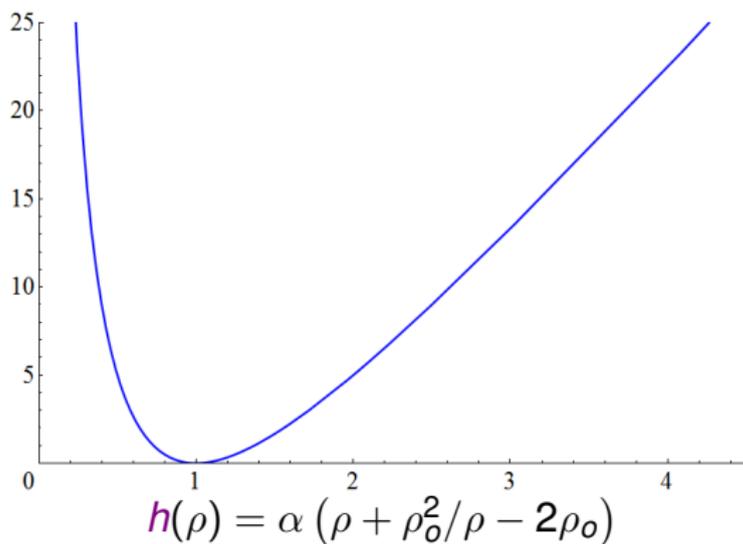
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This gives UGAS, using LaSalle Invariance.

Extra Properties to Achieve All Of Our Goals

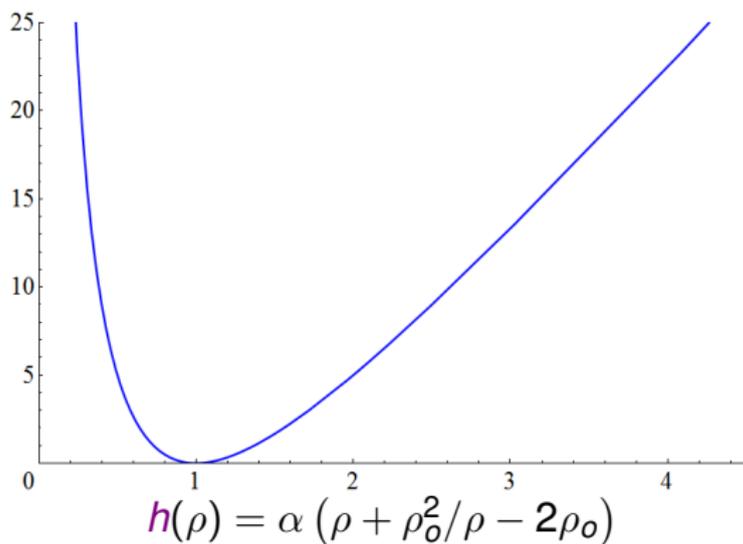
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$$\begin{cases} \dot{\rho} = -\sin(\phi) \\ \dot{\phi} = \frac{\kappa \cos(\phi)}{1+\kappa\rho} + \Gamma[u + \delta] \end{cases} \quad (\rho, \phi) \in \overbrace{(0, \infty) \times (-\pi/2, \pi/2)}^{\text{full state space}} \quad (\Sigma_c)$$

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Control: $\mathbf{u}(\rho, \phi, \hat{\Gamma}) = -\frac{1}{\hat{\Gamma}} \left(\frac{\kappa \cos(\phi)}{1+\kappa\rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi) \right)$ (7)

Estimator: $\dot{\hat{\Gamma}} = (\hat{\Gamma} - \mathbf{c}_{\min})(\mathbf{c}_{\max} - \hat{\Gamma}) \frac{\partial V^\#(\rho, \phi)}{\partial \phi} \mathbf{u}(\rho, \phi, \hat{\Gamma})$ (8)

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$$V^\#(\rho, \phi) = -h'(\rho) \sin(\phi) + \int_0^{V(\rho, \phi)} \gamma(m) dm \quad (9)$$

$$\gamma(q) = \frac{1}{\mu} \left(\frac{2}{\alpha^2 \rho_0^4} (q + 2\alpha\rho_0)^3 + 1 \right) + \frac{\mu}{2} + 2 + \frac{18\alpha}{\rho_0} + \frac{576}{\rho_0^4 \alpha^2} q^3 \quad (10)$$

$$V(\rho, \phi) = -\ln(\cos(\phi)) + h(\rho) \quad (11)$$

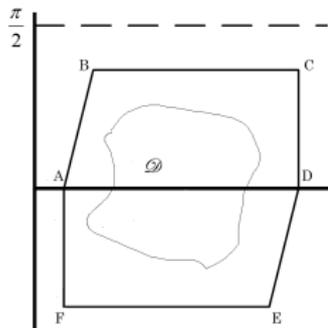
Robustly Forwardly Invariant Hexagonal Regions

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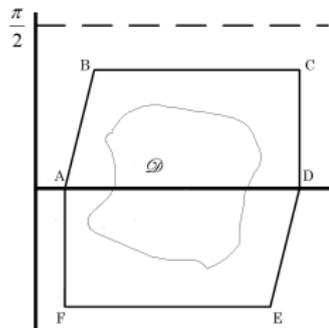
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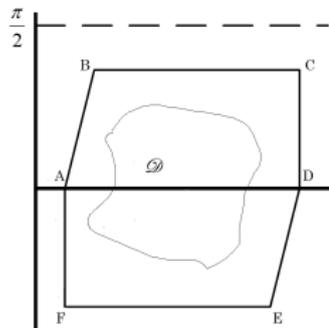
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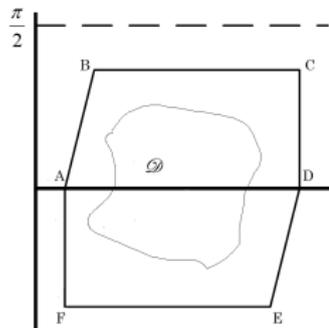


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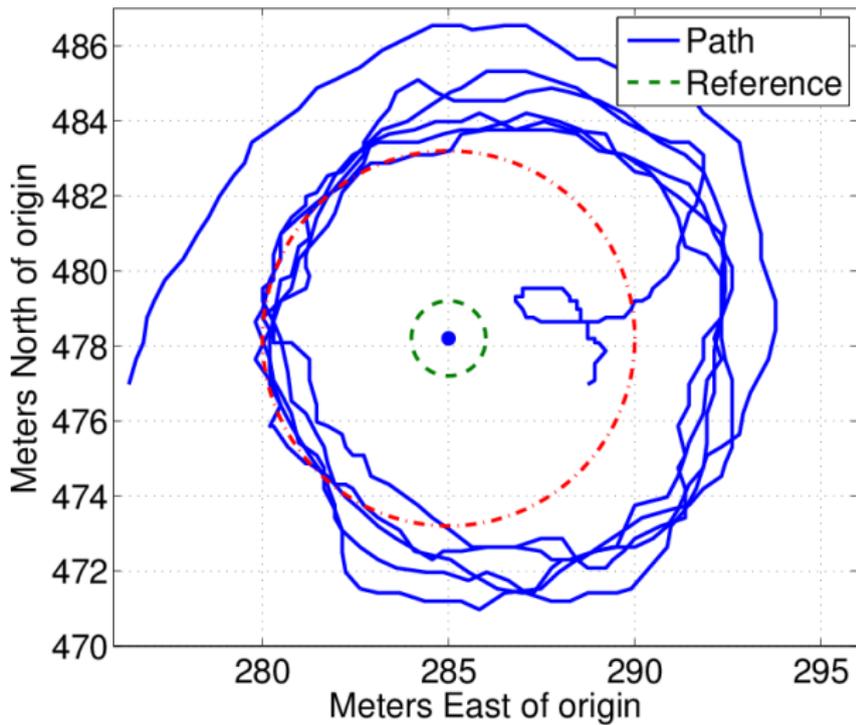
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Georgia Tech Savannah Robotics Team (led by Fumin Zhang).

Field Work at Grand Isle, LA

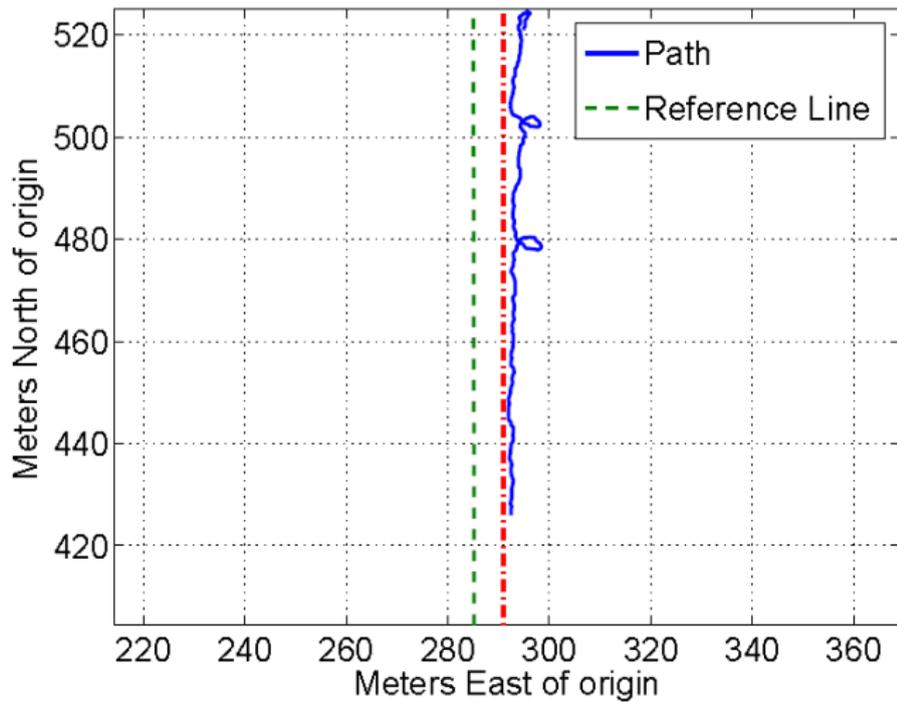
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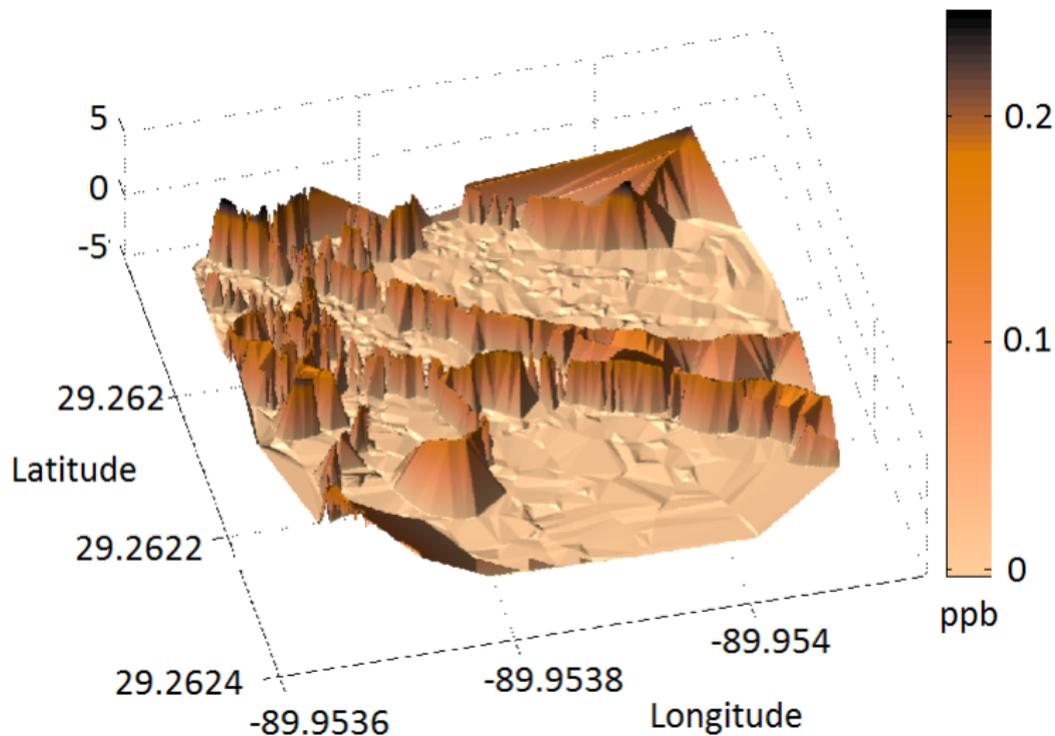
Circle Tracking by ASV Victoria



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Crude Oil Concentration Maps



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In our future work, we will study **adaptive** robust **control** for heterogeneous fleets of autonomous marine vehicles.

References for 2D Case with Hyperlinks

Malisoff, M., F. Mazenc, and F. Zhang, "[Stability and robustness analysis for curve tracking control using input-to-state stability](#)," *IEEE Transactions on Automatic Control*, Volume 57, Issue 5, May 2012, pp. 1320-1326.

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References for 3D Case with Hyperlinks

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