# Adaptive Tracking and Parameter Estimation with Unknown High-Frequency Control Gains: A Case Study in Strictification 

Michael Malisoff, Louisiana State University Joint with Frédéric Mazenc and Marcio de Queiroz Sponsored by AFOSR, NSF/DMS, and NSF/ECCS

SIAM Conference on Control and Its Applications Baltimore, MD - July 25, 2011

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u=u(t, \xi, \hat{\Gamma}), \quad \hat{\Gamma}=\tau(t, \xi, \hat{\Gamma}) \tag{2}
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(iISS)
Find $\gamma_{i}$ 's by building certain strict LFs for $\dot{Y}=\mathcal{G}(t, Y, 0)$.

## Our Work (Nonlinear Analysis TMA, '11)

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- We solved the adaptive tracking and estimation problem for

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\dot{x} & =f(\xi)  \tag{3}\\
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\Gamma=(\theta, \psi)=\left(\theta_{1}, \ldots, \theta_{s}, \psi_{1}, \ldots, \psi_{s}\right) \in \mathbb{R}^{p_{1}+\ldots+p_{s}+s} .
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- The $C^{2} T$-periodic reference trajectory $\xi_{R}=\left(x_{R}, z_{R}\right)$ to be tracked is assumed to satisfy $\dot{x}_{R}(t)=f\left(\xi_{R}(t)\right) \forall t \geq 0$.


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- Main PE Assumption: positive definiteness of the matrices

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\begin{equation*}
\mathcal{P}_{i} \stackrel{\text { def }}{=} \int_{0}^{T} \lambda_{i}^{\top}(t) \lambda_{i}(t) \mathrm{d} t \in \mathbb{R}^{\left(p_{i}+1\right) \times\left(p_{i}+1\right)}, 1 \leq i \leq s \tag{4}
\end{equation*}
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where $\lambda_{i}(t)=\left(k_{i}\left(\xi_{R}(t)\right), \dot{z}_{R, i}(t)-g_{i}\left(\xi_{R}(t)\right)\right)$ for each $i$.

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\begin{equation*}
\underline{\psi}<\psi_{i}<\bar{\psi} \text { and }\left|\theta_{i}\right|<\theta_{M} \tag{6}
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for each $i \in\{1,2, \ldots, s\}$.

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The estimator and feedback can only depend on things we know.

## Augmented Error Dynamics to be Made UGAS

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\dot{\tilde{x}}= & f\left(\tilde{\xi}+\xi_{R}(t)\right)-f\left(\xi_{R}(t)\right)  \tag{10}\\
\dot{\tilde{z}}_{i}= & v_{t, i}(t, \tilde{,})+k_{i}\left(\tilde{\xi}+\xi_{R}(t)\right) \cdot \widetilde{\theta}_{i} \\
& +\widetilde{\psi}_{i} u_{i}(t, \tilde{\xi}, \hat{\theta}, \hat{\psi}), \quad 1 \leq i \leq s \\
\dot{\tilde{\theta}}_{i, j}= & -\left(\hat{\theta}_{i, i}^{2}-\theta_{M}^{2}\right) \varpi_{i, j}, 1 \leq i \leq s, 1 \leq j \leq p_{i} \\
\dot{\tilde{\psi}}_{i}= & -\left(\hat{\psi}_{i}-\underline{\psi}\right)\left(\hat{\psi}_{i}-\bar{\psi}\right) \mho_{i}, 1 \leq i \leq s .
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## Augmented Error Dynamics to be Made UGAS

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\dot{\tilde{x}}= & f\left(\tilde{\xi}+\xi_{R}(t)\right)-f\left(\xi_{R}(t)\right)  \tag{10}\\
\dot{\tilde{z}}_{i}= & v_{t, i}(t, \tilde{\xi})+k_{i}\left(\tilde{\xi}+\xi_{R}(t)\right) \cdot \widetilde{\theta}_{i} \\
& +\widetilde{\psi}_{i} u_{i}(t, \tilde{\xi}, \hat{\theta}, \hat{\psi}), \quad 1 \leq i \leq s \\
\dot{\tilde{\theta}}_{i, j}= & -\left(\hat{\theta}_{\tilde{i}, 2}^{2}-\theta_{M}^{2}\right) \varpi_{i, j}, 1 \leq i \leq s, 1 \leq j \leq p_{i} \\
\tilde{\psi}_{i}= & -\left(\hat{\psi}_{i}-\underline{\psi}\right)\left(\hat{\psi}_{i}-\bar{\psi}\right) \mho_{i}, 1 \leq i \leq s .
\end{align*}\right.
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Tracking error: $\tilde{\xi}=(\tilde{x}, \tilde{z})=\xi-\xi_{R}=\left(x-x_{R}, \underset{\sim}{z}-z_{R}\right)$
Parameter estimation errors: $\widetilde{\theta}_{i}=\theta_{i}-\hat{\theta}_{i}$ and $\widetilde{\psi}_{i}=\psi_{i}-\hat{\psi}_{i}$
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\begin{aligned}
\mathcal{X}= & \mathbb{R}^{r+s} \times\left(\prod_{i=1}^{s}\left\{\prod_{j=1}^{p_{i}}\left(\theta_{i, j}-\theta_{M}, \theta_{i, j}+\theta_{M}\right)\right\}\right) \\
& \times\left(\prod_{i=1}^{s}\left(\psi_{i}-\bar{\psi}, \psi_{i}-\underline{\psi}\right)\right) \subseteq \mathbb{R}^{r+s+p_{1}+\ldots p_{s}+s} .
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## Stabilization Analysis

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- We build a global strict LF for the augmented error $Y=(\tilde{\xi}, \tilde{\theta}, \tilde{\psi})=\left(\xi-\xi_{R}, \theta-\hat{\theta}, \psi-\hat{\psi}\right) \in \mathcal{X}$ dynamics.


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- We start with this nonstrict barrier type LF on $\mathcal{X}$ :

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V_{1}(t, \tilde{\xi}, \tilde{\theta}, \tilde{\psi})= & V(t, \tilde{\xi})+\sum_{i=1}^{s} \sum_{j=1}^{p_{i}} \int_{0}^{\tilde{\theta}_{i, j}} \frac{m}{\theta_{M}^{2}-\left(m-\theta_{i, j}\right)^{2}} \mathrm{~d} m \\
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- On $\mathcal{X}, \dot{V}_{1} \leq-W(\tilde{\xi})$ for some positive definite function $W$.
- This is insufficient for robustness analysis because $V_{1}$ could be zero outside 0 . Therefore, we transform $V_{1}$.


## Transformation from Our Paper

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Theorem: We can construct $K \in \mathcal{K}_{\infty} \cap C^{1}$ such that

$$
\begin{gather*}
V^{\sharp}(t, \tilde{\xi}, \tilde{\theta}, \tilde{\psi})=K\left(V_{1}(t, \tilde{\xi}, \tilde{\theta}, \tilde{\psi})\right)+\sum_{i=1}^{s} \bar{\Upsilon}_{i}(t, \tilde{\xi}, \tilde{\theta}, \tilde{\psi}),  \tag{11}\\
\text { where } \begin{aligned}
\bar{\Upsilon}_{i}(t, \tilde{\xi}, \tilde{\theta}, \tilde{\psi})= & -\tilde{z}_{i} \lambda_{i}(t) \alpha_{i}\left(\widetilde{\theta}_{i}, \widetilde{\psi}_{i}\right) \\
& +\frac{1}{T \bar{\psi}} \alpha_{i}^{\top}\left(\widetilde{\theta}_{i}, \widetilde{\psi}_{i}\right) \Omega_{i}(t) \alpha_{i}\left(\widetilde{\theta}_{i}, \widetilde{\psi}_{i}\right), \\
\lambda_{i}(t)= & \left(k_{i}\left(\xi_{R}(t)\right), \dot{z}_{R, i}(t)-g_{i}\left(\xi_{R}(t)\right)\right), \\
\alpha_{i}\left(\widetilde{\theta}_{i}, \widetilde{\psi}_{i}\right)= & {\left[\begin{array}{c}
\tilde{\theta}_{i} \psi_{i}-\theta_{i} \tilde{\psi}_{i} \\
\widetilde{\psi}_{i}
\end{array}\right], \text { and } } \\
\Omega_{i}(t)= & \int_{t-T}^{t} \int_{m}^{t} \lambda_{i}^{\top}(s) \lambda_{i}(s) \mathrm{d} s \mathrm{~d} m,
\end{aligned} .
\end{gather*}
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is a global strict LF for the $Y$ dynamics on $\mathcal{X}$.

## Application: BLDC Motor (Dawson-Hu-Burg)

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\dot{y}_{1}=y_{2}  \tag{15}\\
\dot{y}_{2}=-\frac{B}{M} y_{2}-\frac{N}{M} \sin \left(y_{1}\right)+K_{T}\left[K_{b} \zeta_{1}+1\right] \zeta_{2} \\
\dot{\zeta}_{i}=H_{i}(y, \zeta) \beta_{i}+\gamma_{i} u_{i}, \quad i=1,2
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- $y_{1}, y_{2}=$ load position and velocity.


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- $y_{1}, y_{2}=$ load position and velocity. $\zeta_{i}=$ winding currents.
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- $B=$ viscous friction coefficient. $M=$ mechanical inertia. $N=$ related to the load mass and gravitational constant. $K_{\tau}, K_{b}=$ torque transmission coefficients.
- The unknown vectors $\beta_{1} \in \mathbb{R}^{2}$ and $\beta_{2} \in \mathbb{R}^{3}$ and unknown scalars $\gamma_{1}$ and $\gamma_{2}$ are the motor electric parameters.

Conclusions

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- We covered systems with unknown control gains including brushless DC motors turning mechanical loads.
- It would be useful to extend to cover models that are not affine in $\Gamma$, feedback delays, and output feedbacks.

