

Asymptotic Stabilization for Feedforward Systems with Delayed Feedbacks

Michael Malisoff, Roy P. Daniels Professor
Louisiana State University Department of Mathematics

JOINT WITH FRÉDÉRIC MAZENC, CR1, INRIA DISCO, L2S CNRS–SUPÉLEC
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$$Y'(t) = \mathcal{G}(t, Y_t, \delta(t)), \quad Y(t) \in \mathcal{Y}, \quad (2)$$

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Fridman, Jankovic, Karafyllis, Krstic, Lin, Teel, ...

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Find γ_i 's by building certain LKFs for $Y'(t) = \mathcal{G}(t, Y_t, 0)$.

Linear Feedforward Systems

Consider the set of all systems having the feedforward form

$$\begin{cases} \dot{x} &= h_1(z) + h_2(z)v(t - \tau) \\ \dot{z} &= f(z) + g(z)v(t - \tau). \end{cases} \quad (3)$$

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The state space is $\mathbb{R}^n \times \mathbb{R}^p$. Linearizing (3) around period τ reference trajectories produces a system of the form

$$\begin{cases} \dot{x}(t) &= C(t)z(t) + D(t)u(t - \tau) \\ \dot{z}(t) &= A(t)z(t) + B(t)u(t - \tau), \end{cases} \quad (4)$$

where A , B , C , and D are C^1 matrix valued functions of period τ .

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We focus on (4), and cases where uncertainties δ are added to u .

Our Two Assumptions

Assumption 1. *The system*

$$\dot{\theta}(t) = A(t)\theta(t) \quad (5)$$

is UGAS. The matrices A , B , C , and D are C^1 and have period τ .

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$$\begin{cases} \frac{\partial \psi_a}{\partial t}(t, m) &= -\psi_a(t, m)A(t) \\ \psi_a(m, m) &= I \end{cases} \quad (6)$$

for all $t \in \mathbb{R}$ and $m \in \mathbb{R}$.

Our Two Assumptions

Lemma

Let Assumption 1 hold. Then the function $I - \psi_a(\ell, \ell - \tau)$ is invertible for all $\ell \in \mathbb{R}$. Also, the function $q : \mathbb{R} \rightarrow \mathbb{R}^{n \times p}$ defined by

$$q(t) = - \int_{t-\tau}^t C(\ell) [I - \psi_a(\ell, \ell - \tau)]^{-1} \psi_a(t, \ell) d\ell \quad (7)$$

has period τ , and $\dot{q}(t) + q(t)A(t) + C(t) = 0$ for all $t \in \mathbb{R}$. \square

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Lemma

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Assumption 2. There exists a constant $c > 0$ such that the matrix $R(t) = q(t)B(t) + D(t)$ satisfies

$$\int_{t-\tau}^t R(m)R(m)^\top dm \geq cI \quad (8)$$

for all $t \in \mathbb{R}$. (That means I is the $n \times n$ identity matrix.)

Main Result

Our coordinate change $\xi(t) = x(t) + q(t)z(t)$ gives

$$\begin{cases} \dot{\xi}(t) &= R(t)u(t - \tau) \\ \dot{z}(t) &= A(t)z(t) + B(t)u(t - \tau) \end{cases} \quad (9)$$

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Theorem

Let Assumptions 1 and 2 hold. Then for all constants $\tau > 0$ and $\epsilon \in (0, \frac{1}{1+4\tau\|R\|^2})$, the controller

$$u(t-\tau) = -\epsilon \frac{R(t-\tau)^\top \xi(t-\tau)}{\sqrt{1+|\xi(t-\tau)|^2}} \quad (10)$$

renders (9) UGAS.

Allowing additive uncertainties on the control gives

$$\begin{cases} \dot{\xi}(t) &= R(t)[u(t - \tau) + \delta(t)] \\ \dot{z}(t) &= A(t)z(t) + B(t)[u(t - \tau) + \delta(t)] . \end{cases} \quad (11)$$

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$$\bar{\delta} = \frac{c}{9k\|R\|(1+2\bar{u})^{1/2}}, \quad \text{where } k = \frac{4\sqrt{2}}{3\epsilon} \left(\tau + \frac{1}{2c}\|R\|^6\tau^4\epsilon^2 \right) \quad (12)$$

$$\text{and } \bar{u} = \max \left\{ \frac{1}{2} + \frac{\epsilon\|R\|^2\tau}{4\sqrt{2}}, \frac{\epsilon\|R\|^2\tau}{4\sqrt{2}} (1 + 2\epsilon\|R\|^2\tau) \right\} .$$

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Theorem

Under the preceding assumptions, (11) in closed loop with

$$\mathbf{u}(t - \tau) = -\epsilon \frac{R(t-\tau)^\top \xi(t-\tau)}{\sqrt{1+|\xi(t-\tau)|^2}} \quad (13)$$

is ISS with respect to the set of all disturbances δ bounded by $\bar{\delta}$.

Application to UAV Dynamics

We study the UAV with standard autopilots which is first order for heading and Mach hold and second order for the altitude hold.

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$$\begin{cases} \dot{x} = v \cos(\theta) \\ \dot{y} = v \sin(\theta) \\ \dot{\theta} = \alpha_{\theta}(\theta_c(t - \tau) - \theta) \\ \dot{v} = \alpha_v(v_c(t - \tau) - v), \end{cases} \quad (14)$$

where we omit the altitude subdynamics $\ddot{h} = -\alpha_h \dot{h} + \alpha_h(h^c - h)$.

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Key Model : Underactuated kino-dynamic representation that is justifiable for high-level formation flight control.

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See e.g. 2004 IEEE-TCST paper by Ren and Beard.

We are given a C^1 reference trajectory $(x_r, y_r, \theta_r, v_r) : \mathbb{R} \rightarrow \mathbb{R}^4$, so there is a reference input $(\theta_{cr}, v_{cr}) : \mathbb{R} \rightarrow \mathbb{R}^2$ such that

$$\begin{cases} \dot{x}_r(t) &= v_r(t) \cos(\theta_r(t)) \\ \dot{y}_r(t) &= v_r(t) \sin(\theta_r(t)) \\ \dot{\theta}_r(t) &= \alpha_\theta(\theta_{cr}(t) - \theta_r(t)) \\ \dot{v}_r(t) &= \alpha_v(v_{cr}(t) - v_r(t)) \end{cases} \quad (15)$$

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Assumption 3 : The functions $\cos(\theta_r(t))$ and $\sin(\theta_r(t))$ have period τ , there exists a constant $t_c \in [0, \tau]$ such that $\dot{\theta}_r(t_c) \neq 0$, and v_r is bounded.

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Tracking Error : $(\bar{x}, \bar{y}, \bar{\theta}, \bar{v}) = (x - x_r, y - y_r, \theta - \theta_r, v - v_r)$.

After a preliminary change of feedbacks, the tracking dynamics are

$$\begin{cases} \dot{\bar{x}} = \cos(\theta_r(t))\bar{v} \\ \quad + [\bar{v} + v_r(t)][\cos(\bar{\theta} + \theta_r(t)) - \cos(\theta_r(t))] \\ \dot{\bar{y}} = \sin(\theta_r(t))\bar{v} \\ \quad + [\bar{v} + v_r(t)][\sin(\bar{\theta} + \theta_r(t)) - \sin(\theta_r(t))] \\ \dot{\bar{v}} = -\alpha_v\bar{v} + \mathbf{u}(t - \tau) \\ \dot{\bar{\theta}} = -\alpha_\theta\bar{\theta}. \end{cases} \quad (16)$$

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$$\begin{aligned} \theta_c(t - \tau) &= \theta_{cr}(t) \quad \text{and} \\ v_c(t - \tau) &= v_{cr}(t) - \frac{\epsilon}{\alpha_v} \frac{R(t-\tau)^\top \xi(t-\tau)}{\sqrt{1+|\xi(t-\tau)|^2}}. \end{aligned} \quad (17)$$

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- Our work applies to a broad class of input delayed feedforward linear systems including a key model for UAVs.
- We can prove global tracking for UAVs under input amplitude constraints, allowing nonperiodic reference trajectories.

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- Our work applies to a broad class of input delayed feedforward linear systems including a key model for UAVs.
- We can prove global tracking for UAVs under input amplitude constraints, allowing nonperiodic reference trajectories.
- It would be interesting to extend the analysis to

$$\begin{cases} \dot{x}(t) &= E(t)x(t) + C(t)z(t) + D(t)u(t - \tau) \\ \dot{z}(t) &= A(t)z(t) + B(t)u(t - \tau). \end{cases} \quad (18)$$

Applications and Conclusions

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Nonlinear analogs involving PDEs would also be interesting.

What is a Lyapunov-Krasovskii Functional (LKF) ?

Definition: We call V^\sharp an ISS-LKF for $Y'(t) = \mathcal{G}(t, Y_t, \delta(t))$ provided there exist functions $\gamma_i \in \mathcal{K}_\infty$ such that:

- 1 $\gamma_1(|\phi(0)|) \leq V^\sharp(t, \phi) \leq \gamma_2(|\phi|_{[-\tau, 0]})$
for all $(t, \phi) \in [0, +\infty) \times \mathcal{C}([-\tau, 0], \mathbb{R}^n)$ and
- 2 $\frac{d}{dt} [V^\sharp(t, Y_t)] \leq -\gamma_3(V^\sharp(t, Y_t)) + \gamma_4(|\delta(t)|)$
along all trajectories of the system

Example: The function $V(Y) = \frac{1}{2}|Y|^2$ is an ISS-LKF for $Y'(t) = -Y(t) + \frac{1}{4}Y(t) + \delta(t)$ for any \mathcal{D} . Fix $\tau > 0$.

$$V^\sharp(Y_t) = V(Y(t)) + \frac{1}{4} \int_{t-\tau}^t |Y(\ell)|^2 d\ell + \frac{1}{8\tau} \int_{t-\tau}^t \left[\int_s^t |Y(r)|^2 dr \right] ds$$

is an ISS-LKF for $Y'(t) = -Y(t) + \frac{1}{4}Y(t - \tau) + \delta(t)$.

Main Result

Our coordinate change $\xi(t) = x(t) + q(t)z(t)$ gave

$$\begin{cases} \dot{\xi}(t) &= R(t)u(t-\tau) \\ \dot{z}(t) &= A(t)z(t) + B(t)u(t-\tau) \end{cases} \quad (19)$$

where $R(t) = q(t)B(t) + D(t)$ and q is from the lemma.

Theorem

Let Assumptions 1 and 2 hold. Then for all constants $\tau > 0$ and $\epsilon \in (0, \frac{1}{1+4\tau\|R\|^2})$, the controller

$$u(t-\tau) = -\epsilon \frac{R(t-\tau)^\top \xi(t-\tau)}{\sqrt{1+|\xi(t-\tau)|^2}} \quad (20)$$

renders (19) UGAS.

Show that the closed loop system (19) admits the LKF

$$V^\#(t, \xi_t, z(t)) = z^\top(t)P(t)z(t) + 21\beta_1 W_3(t, \xi_t), \quad \text{where}$$

$$W_3(t, \xi_t) = W_2(t, \xi_t) + k \left[(1 + 2U(\xi_t))^{3/2} - 1 \right],$$

$$W_2(t, \xi_t) = W_1(t, \xi_t) + \beta_0 \int_{t-\tau}^t \left| \frac{R(m)^\top \xi(m)}{\sqrt{1 + |\xi(m)|^2}} \right|^2 dm,$$

$$W_1(t, \xi_t) = \xi(t)^\top \left[\int_{t-\tau}^t \int_m^t R(\ell)R(\ell)^\top d\ell dm \right] \xi(t),$$

$$U(\xi_t) = \frac{1}{2}|\xi|^2 + \frac{1}{4\tau} \int_{t-2\tau}^t \int_m^t \frac{\epsilon |R(\ell)^\top \xi(\ell)|^2}{2\sqrt{2}\sqrt{1 + |\xi(\ell)|^2}} d\ell dm,$$

$$\beta_0 = \frac{1}{2c} \|R\|^6 \tau^4 \epsilon^2, \quad k = \frac{4\sqrt{2}}{3\epsilon} (\tau + \beta_0),$$

$$\beta_1 = \max\{v_1, v_2\}, \quad v_1 = \frac{2}{c} [4\|P\|^2 \|B\|^2 \|R\|^2 + 1],$$

$$\text{and } v_2 = \frac{16\sqrt{2}\tau}{3\epsilon k} (1 + 8\tau\|P\|^2 \|B\|^2 \|R\|^4).$$