Curve Tracking for Marine Robots: A Case Study in Feedback Control

Michael Malisoff, Louisiana State University
Sponsor: NSF Energy, Power, and Adaptive Systems
Joint with Georgia Tech Savannah Robotics Team

Department of EECS Seminar Northwestern University – July 2014

These are *triply* parameterized families of ODEs of the form

$$Y'(t) = \mathcal{F}(t, Y(t), \mathbf{u}(t, Y(t - \tau)), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}.$$
 (1)

These are *triply* parameterized families of ODEs of the form

$$Y'(t) = \mathcal{F}(t, Y(t), \mathbf{u}(t, Y(t - \tau)), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}.$$
 (1)

 $\mathcal{Y} \subseteq \mathbb{R}^n$.

These are triply parameterized families of ODEs of the form

$$Y'(t) = \mathcal{F}(t, Y(t), \mathbf{u}(t, Y(t - \tau)), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}.$$
 (1)

 $\mathcal{Y} \subseteq \mathbb{R}^n$. We have freedom to choose the control function $\underline{\mathbf{u}}$.

These are *triply* parameterized families of ODEs of the form

$$Y'(t) = \mathcal{F}(t, Y(t), \mathbf{u}(t, Y(t - \tau)), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}.$$
 (1)

 $\mathcal{Y} \subseteq \mathbb{R}^n$. We have freedom to choose the control function \underline{u} . The functions $\delta : [0, \infty) \to \mathcal{D}$ represent uncertainty.

These are *triply* parameterized families of ODEs of the form

$$Y'(t) = \mathcal{F}(t, Y(t), \mathbf{u}(t, Y(t - \tau)), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}.$$
 (1)

 $\mathcal{Y} \subseteq \mathbb{R}^n$. We have freedom to choose the control function $\underline{\mathbf{u}}$. The functions $\delta : [0, \infty) \to \mathcal{D}$ represent uncertainty. $\mathcal{D} \subseteq \mathbb{R}^m$.

These are *triply* parameterized families of ODEs of the form

$$Y'(t) = \mathcal{F}(t, Y(t), \mathbf{u}(t, Y(t - \tau)), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}. \tag{1}$$

 $\mathcal{Y} \subseteq \mathbb{R}^n$. We have freedom to choose the control function \underline{u} . The functions $\delta : [0, \infty) \to \mathcal{D}$ represent uncertainty. $\mathcal{D} \subseteq \mathbb{R}^m$. The vector Γ is constant but unknown.

These are triply parameterized families of ODEs of the form

$$Y'(t) = \mathcal{F}(t, Y(t), \mathbf{u}(t, Y(t - \tau)), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}. \tag{1}$$

 $\mathcal{Y} \subseteq \mathbb{R}^n$. We have freedom to choose the control function \underline{u} . The functions $\delta : [0, \infty) \to \mathcal{D}$ represent uncertainty. $\mathcal{D} \subseteq \mathbb{R}^m$. The vector Γ is constant but unknown. $\underline{\tau}$ is a constant delay.

These are triply parameterized families of ODEs of the form

$$Y'(t) = \mathcal{F}(t, Y(t), \mathbf{u}(t, Y(t - \tau)), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}.$$
 (1)

 $\mathcal{Y} \subseteq \mathbb{R}^n$. We have freedom to choose the control function \underline{u} . The functions $\delta : [0, \infty) \to \mathcal{D}$ represent uncertainty. $\mathcal{D} \subseteq \mathbb{R}^m$. The vector Γ is constant but unknown. $\underline{\tau}$ is a constant delay.

Specify u to get a doubly parameterized closed loop family

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y},$$
 (2)

where $\mathcal{G}(t, Y(t), Y(t-\tau), \Gamma, d) = \mathcal{F}(t, Y(t), \mathbf{u}(t, Y(t-\tau)), \Gamma, d)$.

These are *triply* parameterized families of ODEs of the form

$$Y'(t) = \mathcal{F}(t, Y(t), \mathbf{u}(t, Y(t-\tau)), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}.$$
 (1)

 $\mathcal{Y} \subseteq \mathbb{R}^n$. We have freedom to choose the control function \underline{u} . The functions $\delta:[0,\infty)\to\mathcal{D}$ represent uncertainty. $\mathcal{D}\subseteq\mathbb{R}^m$. The vector Γ is constant but unknown. $\underline{\tau}$ is a constant delay.

Specify *u* to get a *doubly* parameterized closed loop family

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}, \tag{2}$$

where
$$\mathcal{G}(t, Y(t), Y(t - \tau), \Gamma, d) = \mathcal{F}(t, Y(t), \mathbf{u}(t, Y(t - \tau)), \Gamma, d)$$
.

Typically we construct \underline{u} such that all trajectories of (2) for all possible choices of δ satisfy some control objective.

Input-to-state stability generalizes global asymptotic stability.

Input-to-state stability generalizes global asymptotic stability.

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma), \quad Y(t) \in \mathcal{Y}$$
 (\(\Sigma\)

Input-to-state stability generalizes global asymptotic stability.

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma), \quad Y(t) \in \mathcal{Y}$$

$$|Y(t)| \le \gamma_1 \left(e^{t_0 - t} \gamma_2(|Y|_{[t_0 - \tau, t_0]}) \right)$$
(UGAS)

Input-to-state stability generalizes global asymptotic stability.

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma), \quad Y(t) \in \mathcal{Y}$$

$$|Y(t)| \le \gamma_1 \left(e^{t_0 - t} \gamma_2(|Y|_{[t_0 - \tau, t_0]}) \right)$$
(UGAS)

Our γ_i 's are 0 at 0, strictly increasing, and unbounded.

Input-to-state stability generalizes global asymptotic stability.

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma), \quad Y(t) \in \mathcal{Y}$$

$$|Y(t)| \le \gamma_1 \left(e^{t_0 - t} \gamma_2 (|Y|_{[t_0 - \tau, t_0]}) \right)$$
(UGAS)

Our γ_i 's are 0 at 0, strictly increasing, and unbounded. $\gamma_i \in \mathcal{K}_{\infty}$.

Input-to-state stability generalizes global asymptotic stability.

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma), \quad Y(t) \in \mathcal{Y}$$

$$|Y(t)| \le \gamma_1 \left(e^{t_0 - t} \gamma_2 (|Y|_{[t_0 - \tau, t_0]}) \right)$$
(UGAS)

Our γ_i 's are 0 at 0, strictly increasing, and unbounded. $\gamma_i \in \mathcal{K}_{\infty}$.

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}$$
 (Σ_{pert})

Input-to-state stability generalizes global asymptotic stability.

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma), \quad Y(t) \in \mathcal{Y}$$

$$|Y(t)| \le \gamma_1 \left(e^{t_0 - t} \gamma_2 (|Y|_{\lceil t_0 - \tau, t_0 \rceil}) \right)$$
(UGAS)

Our γ_i 's are 0 at 0, strictly increasing, and unbounded. $\gamma_i \in \mathcal{K}_{\infty}$.

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}$$
 (Σ_{pert})

$$|Y(t)| \le \gamma_1 \left(e^{t_0 - t} \gamma_2(|Y|_{[t_0 - \tau, t_0]}) \right) + \gamma_3(|\delta|_{[t_0, t]})$$
 (ISS)

Input-to-state stability generalizes global asymptotic stability.

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma), \quad Y(t) \in \mathcal{Y}$$
 (\(\Sigma\)

$$|\mathit{Y}(\mathit{t})| \leq \gamma_1 \left(e^{\mathit{t}_0 - \mathit{t}} \gamma_2 (|\mathit{Y}|_{[\mathit{t}_0 - \tau, \mathit{t}_0]}) \right) \tag{UGAS}$$

Our γ_i 's are 0 at 0, strictly increasing, and unbounded. $\gamma_i \in \mathcal{K}_{\infty}$.

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma, \delta(t)), Y(t) \in \mathcal{Y}$$
 (Σ_{pert})

$$|Y(t)| \le \gamma_1 \left(e^{t_0 - t} \gamma_2(|Y|_{[t_0 - \tau, t_0]}) \right) + \gamma_3(|\delta|_{[t_0, t]})$$
 (ISS)

Find γ_i 's by building special strict Lyapunov functions.

Input-to-state stability generalizes global asymptotic stability.

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma), \quad Y(t) \in \mathcal{Y}$$
 (\(\Sigma\)

$$|\mathit{Y}(\mathit{t})| \leq \gamma_1 \left(e^{\mathit{t}_0 - \mathit{t}} \gamma_2 (|\mathit{Y}|_{[\mathit{t}_0 - \tau, \mathit{t}_0]}) \right) \tag{UGAS}$$

Our γ_i 's are 0 at 0, strictly increasing, and unbounded. $\gamma_i \in \mathcal{K}_{\infty}$.

$$Y'(t) = \mathcal{G}(t, Y(t), Y(t - \tau), \Gamma, \delta(t)), \quad Y(t) \in \mathcal{Y}$$
 (Σ_{pert})

$$|Y(t)| \le \gamma_1 \left(e^{t_0 - t} \gamma_2(|Y|_{[t_0 - \tau, t_0]}) \right) + \gamma_3(|\delta|_{[t_0, t]})$$
 (ISS)

Find γ_i 's by building special strict Lyapunov functions.

Ex: When $\tau = 0$, Σ_{pert} is ISS iff it has an ISS Lf (Sontag-Wang).

Active magnetic bearings, bioreactors, brushless DC motors, heart rate controllers, marine robots, microelectromechanical relays, neuromuscular electrical stimulation, underactuated ships, unmanned air vehicles,..

Active magnetic bearings, bioreactors, brushless DC motors, heart rate controllers, marine robots, microelectromechanical relays, neuromuscular electrical stimulation, underactuated ships, unmanned air vehicles,..

For many systems, we design controls $\underline{\textbf{\textit{u}}}$ that ensure ISS under the delays $\underline{\textbf{\textit{\tau}}}$ and uncertainties δ that prevail in engineering.

Active magnetic bearings, bioreactors, brushless DC motors, heart rate controllers, marine robots, microelectromechanical relays, neuromuscular electrical stimulation, underactuated ships, unmanned air vehicles,..

For many systems, we design controls $\underline{\textbf{\textit{u}}}$ that ensure ISS under the delays $\underline{\textbf{\textit{\tau}}}$ and uncertainties δ that prevail in engineering.

We combine the plants with dynamics for parameter estimators $\hat{\Gamma}(t)$ that converge to Γ , and then use $\hat{\Gamma}(t)$ in u, instead of Γ .

Active magnetic bearings, bioreactors, brushless DC motors, heart rate controllers, marine robots, microelectromechanical relays, neuromuscular electrical stimulation, underactuated ships, unmanned air vehicles,..

For many systems, we design controls $\underline{\textbf{\textit{u}}}$ that ensure ISS under the delays $\underline{\textbf{\textit{\tau}}}$ and uncertainties δ that prevail in engineering.

We combine the plants with dynamics for parameter estimators $\hat{\Gamma}(t)$ that converge to Γ , and then use $\hat{\Gamma}(t)$ in u, instead of Γ .

For state constrained systems, we choose $\mathcal Y$ to find maximal perturbation sets $\mathcal D$ the system can tolerate without leaving $\mathcal Y$.

Active magnetic bearings, bioreactors, brushless DC motors, heart rate controllers, marine robots, microelectromechanical relays, neuromuscular electrical stimulation, underactuated ships, unmanned air vehicles,..

For many systems, we design controls $\underline{\textbf{\textit{u}}}$ that ensure ISS under the delays $\underline{\textbf{\textit{\tau}}}$ and uncertainties δ that prevail in engineering.

We combine the plants with dynamics for parameter estimators $\hat{\Gamma}(t)$ that converge to Γ , and then use $\hat{\Gamma}(t)$ in u, instead of Γ .

For state constrained systems, we choose \mathcal{Y} to find maximal perturbation sets \mathcal{D} the system can tolerate without leaving \mathcal{Y} .

To handle delays τ , we transform nonstrict Lyapunov functions into strict ones, and then into Lyapunov-Krasovskii functionals.

Active magnetic bearings, bioreactors, brushless DC motors, heart rate controllers, marine robots, microelectromechanical relays, neuromuscular electrical stimulation, underactuated ships, unmanned air vehicles,..

For many systems, we design controls ${\it u}$ that ensure ISS under the delays ${\it \tau}$ and uncertainties δ that prevail in engineering.

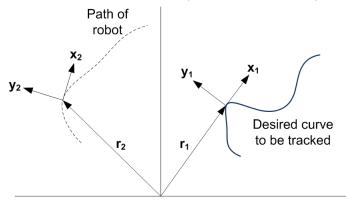
We combine the plants with dynamics for parameter estimators $\hat{\Gamma}(t)$ that converge to Γ , and then use $\hat{\Gamma}(t)$ in u, instead of Γ .

For state constrained systems, we choose \mathcal{Y} to find maximal perturbation sets \mathcal{D} the system can tolerate without leaving \mathcal{Y} .

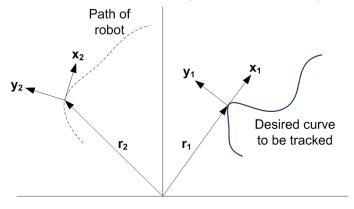
To handle delays τ , we transform nonstrict Lyapunov functions into strict ones, and then into Lyapunov-Krasovskii functionals.

Motivation: Pollutants from Deepwater Horizon oil spill.

Motivation: Pollutants from Deepwater Horizon oil spill.



Motivation: Pollutants from Deepwater Horizon oil spill.



$$ho = |\mathbf{r_2} - \mathbf{r_1}|, \, \phi = \text{angle between } \mathbf{x_1} \text{ and } \mathbf{x_2}, \, \cos(\phi) = \mathbf{x_1} \cdot \mathbf{x_2}$$

Interaction of a unit speed robot and its projection on the curve.

Interaction of a unit speed robot and its projection on the curve.

$$\dot{\rho} = -\sin\phi, \quad \dot{\phi} = \frac{\kappa\cos\phi}{1+\kappa\rho} - \frac{\mathbf{u_2}}{1}, \quad (\rho,\phi) \in \mathcal{X} \ .$$

Interaction of a unit speed robot and its projection on the curve.

$$\dot{\rho} = -\sin\phi, \quad \dot{\phi} = \frac{\kappa\cos\phi}{1+\kappa\rho} - \frac{\mathbf{u_2}}{2}, \quad (\rho,\phi) \in \mathcal{X} \ .$$
 (S)

 $\rho =$ relative distance.

Interaction of a unit speed robot and its projection on the curve.

$$\dot{\rho} = -\sin\phi, \quad \dot{\phi} = \frac{\kappa\cos\phi}{1+\kappa\rho} - \frac{\mathbf{U_2}}{2}, \quad (\rho,\phi) \in \mathcal{X} \; .$$

 $\rho = \text{relative distance.} \ \phi = \text{bearing.}$

Interaction of a unit speed robot and its projection on the curve.

$$\dot{
ho} = -\sin\phi, \quad \dot{\phi} = rac{\kappa\cos\phi}{1+\kappa
ho} - rac{m{u_2}}{2} \,, \;\; (
ho,\phi) \in \mathcal{X} \;. \eqno(\Sigma)$$

$$\rho = \text{relative distance}. \ \phi = \text{bearing}. \ \mathcal{X} = (0, +\infty) \times (-\pi/2, \pi/2).$$

Interaction of a unit speed robot and its projection on the curve.

$$\dot{
ho} = -\sin\phi, \quad \dot{\phi} = rac{\kappa\cos\phi}{1+\kappa
ho} - rac{m{
u_2}}{2} \,, \ (
ho,\phi) \in \mathcal{X} \,.$$

 $\rho = \text{relative distance.} \ \phi = \text{bearing.} \ \mathcal{X} = (0, +\infty) \times (-\pi/2, \pi/2).$ $\kappa = \text{positive curvature at the closest point.}$

Interaction of a unit speed robot and its projection on the curve.

 $\rho=$ relative distance. $\phi=$ bearing. $\mathcal{X}=(0,+\infty)\times(-\pi/2,\pi/2).$ $\kappa=$ positive curvature at the closest point. $\mathbf{u_2}=$ steering control.

Interaction of a unit speed robot and its projection on the curve.

 $\rho=$ relative distance. $\phi=$ bearing. $\mathcal{X}=(0,+\infty)\times(-\pi/2,\pi/2).$ $\kappa=$ positive curvature at the closest point. $\mathbf{u_2}=$ steering control.

Lumelsky-Stepanov.

Interaction of a unit speed robot and its projection on the curve.

 $\rho =$ relative distance. $\phi =$ bearing. $\mathcal{X} = (0, +\infty) \times (-\pi/2, \pi/2)$. $\kappa =$ positive curvature at the closest point. $u_2 =$ steering control.

Lumelsky-Stepanov. Micaelli-Samson.

Interaction of a unit speed robot and its projection on the curve.

$$\dot{\rho} = -\sin\phi, \quad \dot{\phi} = \frac{\kappa\cos\phi}{1+\kappa\rho} - \frac{\mathbf{u_2}}{2}, \quad (\rho,\phi) \in \mathcal{X}.$$

 $\rho=$ relative distance. $\phi=$ bearing. $\mathcal{X}=(0,+\infty)\times(-\pi/2,\pi/2).$ $\kappa=$ positive curvature at the closest point. $\mathbf{u_2}=$ steering control.

Lumelsky-Stepanov. Micaelli-Samson. Morin-Samson.

Interaction of a unit speed robot and its projection on the curve.

 $\rho=$ relative distance. $\phi=$ bearing. $\mathcal{X}=(0,+\infty)\times(-\pi/2,\pi/2).$ $\kappa=$ positive curvature at the closest point. $\mathbf{u_2}=$ steering control.

Lumelsky-Stepanov. Micaelli-Samson. Morin-Samson. Zhang...

Interaction of a unit speed robot and its projection on the curve.

 $\rho=$ relative distance. $\phi=$ bearing. $\mathcal{X}=(0,+\infty)\times(-\pi/2,\pi/2).$ $\kappa=$ positive curvature at the closest point. $\mathbf{u_2}=$ steering control.

Lumelsky-Stepanov. Micaelli-Samson. Morin-Samson. Zhang..

Control Objectives in Undelayed Nonadaptive Case:

Interaction of a unit speed robot and its projection on the curve.

 $\rho=$ relative distance. $\phi=$ bearing. $\mathcal{X}=(0,+\infty)\times(-\pi/2,\pi/2).$ $\kappa=$ positive curvature at the closest point. $\mathbf{u_2}=$ steering control.

Lumelsky-Stepanov. Micaelli-Samson. Morin-Samson. Zhang..

Control Objectives in Undelayed Nonadaptive Case:

(A) Design u_2 to get UGAS of an equilibrium $\mathcal{E} = (\rho_0, 0)$.

Interaction of a unit speed robot and its projection on the curve.

$$\dot{
ho} = -\sin\phi, \quad \dot{\phi} = rac{\kappa\cos\phi}{1+\kappa\rho} - rac{m{
u_2}}{2} \; , \; \; (
ho,\phi) \in \mathcal{X} \; .$$

 $\rho=$ relative distance. $\phi=$ bearing. $\mathcal{X}=(0,+\infty)\times(-\pi/2,\pi/2).$ $\kappa=$ positive curvature at the closest point. $\mathbf{u_2}=$ steering control.

Lumelsky-Stepanov. Micaelli-Samson. Morin-Samson. Zhang..

Control Objectives in Undelayed Nonadaptive Case:

- (A) Design u_2 to get UGAS of an equilibrium $\mathcal{E} = (\rho_0, 0)$.
- (B) Prove ISS properties under actuator errors δ added to u_2 .

Interaction of a unit speed robot and its projection on the curve.

$$\dot{\rho} = -\sin\phi, \quad \dot{\phi} = \frac{\kappa\cos\phi}{1+\kappa\rho} - \frac{\mathbf{u_2}}{2}, \quad (\rho,\phi) \in \mathcal{X}.$$
 (S)

 $\rho=$ relative distance. $\phi=$ bearing. $\mathcal{X}=(0,+\infty)\times(-\pi/2,\pi/2)$. $\kappa=$ positive curvature at the closest point. $\mathbf{u_2}=$ steering control.

Lumelsky-Stepanov. Micaelli-Samson. Morin-Samson. Zhang..

Control Objectives in Undelayed Nonadaptive Case:

- (A) Design u_2 to get UGAS of an equilibrium $\mathcal{E} = (\rho_0, 0)$.
- (B) Prove ISS properties under actuator errors δ added to u_2 .

ISS:
$$|(\rho,\phi)(t)|_{\mathcal{E}} \leq \gamma_1(\gamma_2(|(\rho,\phi)(0)|_{\mathcal{E}})e^{-ct}) + \gamma_3(|\delta|_{[0,t]}).$$

Interaction of a unit speed robot and its projection on the curve.

$$\dot{\rho} = -\sin\phi, \quad \dot{\phi} = \frac{\kappa\cos\phi}{1+\kappa\rho} - \frac{\mathbf{u_2}}{1}, \quad (\rho,\phi) \in \mathcal{X} \ .$$

 $\rho=$ relative distance. $\phi=$ bearing. $\mathcal{X}=(0,+\infty)\times(-\pi/2,\pi/2)$. $\kappa=$ positive curvature at the closest point. $\mathbf{u_2}=$ steering control.

Lumelsky-Stepanov. Micaelli-Samson. Morin-Samson. Zhang..

Control Objectives in Undelayed Nonadaptive Case:

- (A) Design u_2 to get UGAS of an equilibrium $\mathcal{E} = (\rho_0, 0)$.
- (B) Prove ISS properties under actuator errors δ added to u_2 .

ISS:
$$|(\rho,\phi)(t)|_{\mathcal{E}} \leq \gamma_1 (\gamma_2(|(\rho,\phi)(0)|_{\mathcal{E}})e^{-ct}) + \gamma_3(|\delta|_{[0,t]}).$$

Feedback linearization with $z = \sin(\phi)$ cannot be applied.

They realized Control Objective (A) using controllers of the form

$$u_2 = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi). \tag{3}$$

They realized Control Objective (A) using controllers of the form

$$u_2 = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi). \tag{3}$$

Assumption 1:

They realized Control Objective (A) using controllers of the form

$$\mathbf{U_2} = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi). \tag{3}$$

Assumption 1: $h:(0,+\infty)\to [0,\infty)$ is C^1

They realized Control Objective (A) using controllers of the form

$$\mathbf{U_2} = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi). \tag{3}$$

Assumption 1: $h:(0,+\infty)\to [0,\infty)$ is C^1 , h' has only finitely many zeros

They realized Control Objective (A) using controllers of the form

$$u_2 = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi). \tag{3}$$

Assumption 1: $h:(0,+\infty)\to [0,\infty)$ is C^1 , h' has only finitely many zeros, $\lim_{\rho\to 0^+}h(\rho)=\lim_{\rho\to\infty}h(\rho)=\infty$

They realized Control Objective (A) using controllers of the form

$$\mathbf{U_2} = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi). \tag{3}$$

Assumption 1: $h: (0, +\infty) \to [0, \infty)$ is C^1 , h' has only finitely many zeros, $\lim_{\rho \to 0^+} h(\rho) = \lim_{\rho \to \infty} h(\rho) = \infty$, and $h \in \mathcal{PD}(\rho_0)$.

They realized Control Objective (A) using controllers of the form

$$u_2 = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi). \tag{3}$$

Assumption 1: $h: (0, +\infty) \to [0, \infty)$ is C^1 , h' has only finitely many zeros, $\lim_{\rho \to 0^+} h(\rho) = \lim_{\rho \to \infty} h(\rho) = \infty$, and $h \in \mathcal{PD}(\rho_0)$.

Strategy:

They realized Control Objective (A) using controllers of the form

$$\mathbf{U_2} = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi). \tag{3}$$

Assumption 1: $h: (0, +\infty) \to [0, \infty)$ is C^1 , h' has only finitely many zeros, $\lim_{\rho \to 0^+} h(\rho) = \lim_{\rho \to \infty} h(\rho) = \infty$, and $h \in \mathcal{PD}(\rho_0)$.

Strategy: Use the Lyapunov function candidate

$$V(\rho,\phi) = -\ln\left(\cos(\phi)\right) + h(\rho). \tag{4}$$

They realized Control Objective (A) using controllers of the form

$$\mathbf{U_2} = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi). \tag{3}$$

Assumption 1: $h: (0, +\infty) \to [0, \infty)$ is C^1 , h' has only finitely many zeros, $\lim_{\rho \to 0^+} h(\rho) = \lim_{\rho \to \infty} h(\rho) = \infty$, and $h \in \mathcal{PD}(\rho_0)$.

Strategy: Use the Lyapunov function candidate

$$V(\rho,\phi) = -\ln\left(\cos(\phi)\right) + h(\rho). \tag{4}$$

Along $\dot{\rho} = -\sin(\phi)$, $\dot{\phi} = h'(\rho)\cos(\phi) - \mu\sin(\phi)$, we get

$$\dot{V} = -\mu \frac{\sin^2(\phi)}{\cos(\phi)} \le 0 . \tag{5}$$

They realized Control Objective (A) using controllers of the form

$$\mathbf{U_2} = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi). \tag{3}$$

Assumption 1: $h: (0, +\infty) \to [0, \infty)$ is C^1 , h' has only finitely many zeros, $\lim_{\rho \to 0^+} h(\rho) = \lim_{\rho \to \infty} h(\rho) = \infty$, and $h \in \mathcal{PD}(\rho_0)$.

Strategy: Use the Lyapunov function candidate

$$V(\rho,\phi) = -\ln\left(\cos(\phi)\right) + h(\rho). \tag{4}$$

Along $\dot{\rho} = -\sin(\phi)$, $\dot{\phi} = h'(\rho)\cos(\phi) - \mu\sin(\phi)$, we get

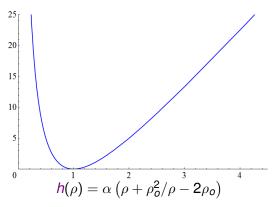
$$\dot{V} = -\mu \frac{\sin^2(\phi)}{\cos(\phi)} \le 0 . \tag{5}$$

This gives global asymptotic stability, using LaSalle Invariance.

Extra Properties to Achieve All Of Our Goals

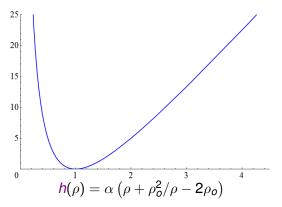
Extra Properties to Achieve All Of Our Goals

To realize our goals, we added assumptions on h which hold for



Extra Properties to Achieve All Of Our Goals

To realize our goals, we added assumptions on h which hold for



See my Automatica and TAC papers with Fumin Zhang.

$$\begin{cases} \dot{\rho} = -\sin(\phi) \\ \dot{\phi} = \frac{\kappa\cos(\phi)}{1+\kappa\rho} + \Gamma[\underline{u}+\delta] \end{cases} \qquad (\rho,\phi) \in \overbrace{(0,\infty)\times(-\pi/2,\pi/2)}^{\text{full state space}} \qquad (\Sigma_c)$$

$$\begin{cases} \dot{\rho} = -\sin(\phi) \\ \dot{\phi} = \frac{\kappa\cos(\phi)}{1+\kappa\rho} + \Gamma[\frac{\mathbf{u}}{1} + \delta] \end{cases} \qquad (\rho, \phi) \in \overbrace{(0, \infty) \times (-\pi/2, \pi/2)}^{\text{full state space}} \qquad (\Sigma_c)$$

Control:
$$u(\rho, \phi, \hat{\Gamma}) = -\frac{1}{\hat{\Gamma}} \left(\frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi) \right)$$
 (6)

Estimator:
$$\hat{\Gamma} = (\hat{\Gamma} - c_{\min})(c_{\max} - \hat{\Gamma}) \frac{\partial V^{\sharp}(\rho,\phi)}{\partial \phi} u(\rho,\phi,\hat{\Gamma})$$
 (7)

$$\begin{cases} \dot{\rho} = -\sin(\phi) \\ \dot{\phi} = \frac{\kappa\cos(\phi)}{1+\kappa\rho} + \Gamma[\frac{\textbf{\textit{u}}}{1} + \delta] \end{cases} \qquad (\rho, \phi) \in \overbrace{(0, \infty) \times (-\pi/2, \pi/2)}^{\text{full state space}} \qquad (\Sigma_c)$$

Control:
$$u(\rho, \phi, \hat{\Gamma}) = -\frac{1}{\hat{\Gamma}} \left(\frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi) \right)$$
 (6)

Estimator:
$$\hat{\Gamma} = (\hat{\Gamma} - c_{\min})(c_{\max} - \hat{\Gamma}) \frac{\partial V^{\sharp}(\rho,\phi)}{\partial \phi} u(\rho,\phi,\hat{\Gamma})$$
 (7)

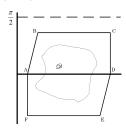
$$V^{\sharp}(\rho,\phi) = -h'(\rho)\sin(\phi) + \int_{0}^{V(\rho,\phi)} \gamma(m)dm$$
 (8)

$$\gamma(q) = \frac{1}{\mu} \left(\frac{2}{\alpha^2 \rho_0^4} (q + 2\alpha \rho_0)^3 + 1 \right) + \frac{\mu}{2} + 2 + \frac{18\alpha}{\rho_0} + \frac{576}{\rho_0^4 \alpha^2} q^3$$
 (9)

$$V(\rho,\phi) = -\ln\left(\cos(\phi)\right) + h(\rho) \tag{10}$$

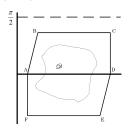
We must restrict the suprema of the perturbations $\delta(t)$ to keep (ρ, ϕ) from exiting $\mathcal{X} = (0, \infty) \times (-\pi/2, \pi/2)$.

We must restrict the suprema of the perturbations $\delta(t)$ to keep (ρ, ϕ) from exiting $\mathcal{X} = (0, \infty) \times (-\pi/2, \pi/2)$.



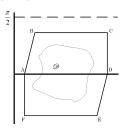
View the state space $(0,\infty) \times (-\pi/2,\pi/2)$ as a union of compact hexagonally shaped regions $H_1 \subseteq H_2 \subseteq \ldots \subseteq H_i \subseteq \ldots$

We must restrict the suprema of the perturbations $\delta(t)$ to keep (ρ, ϕ) from exiting $\mathcal{X} = (0, \infty) \times (-\pi/2, \pi/2)$.



View the state space $(0,\infty)\times (-\pi/2,\pi/2)$ as a union of compact hexagonally shaped regions $H_1\subseteq H_2\subseteq\ldots\subseteq H_i\subseteq\ldots$ [For each i, all trajectories of (Σ_c) starting in H_i for all $\delta:[0,\infty)\to[-\delta_{*i},\delta_{*i}]$ stay in H_i .] The tilted legs have slope $c_{\min}\mu/c_{\max}$.

We must restrict the suprema of the perturbations $\delta(t)$ to keep (ρ, ϕ) from exiting $\mathcal{X} = (0, \infty) \times (-\pi/2, \pi/2)$.

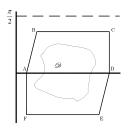


View the state space $(0,\infty)\times (-\pi/2,\pi/2)$ as a union of compact hexagonally shaped regions $H_1\subseteq H_2\subseteq\ldots\subseteq H_i\subseteq\ldots$ [For each i, all trajectories of (Σ_c) starting in H_i for all $\delta:[0,\infty)\to[-\delta_{*i},\delta_{*i}]$ stay in H_i .] The tilted legs have slope $c_{\min}\mu/c_{\max}$.

For each index i, we take δ_{*i} to be the largest allowable disturbance bound to maintain forward invariance of H_i .

Robustly Forwardly Invariant Hexagonal Regions

We must restrict the suprema of the perturbations $\delta(t)$ to keep (ρ, ϕ) from exiting $\mathcal{X} = (0, \infty) \times (-\pi/2, \pi/2)$.



View the state space $(0,\infty) \times (-\pi/2,\pi/2)$ as a union of compact hexagonally shaped regions $H_1 \subseteq H_2 \subseteq \ldots \subseteq H_i \subseteq \ldots$ [For each i, all trajectories of (Σ_c) starting in H_i for all $\delta: [0,\infty) \to [-\delta_{*i},\delta_{*i}]$ stay in H_i .] The tilted legs have slope $c_{\min}\mu/c_{\max}$.

For each index i, we take δ_{*i} to be the largest allowable disturbance bound to maintain forward invariance of H_i .

Then we prove ISS of the tracking and parameter identification dynamics for each set H_i and the disturbance set $\mathcal{D} = [-\delta_{*i}, \delta_{*i}]$.





20 days of field work off Grand Isle.



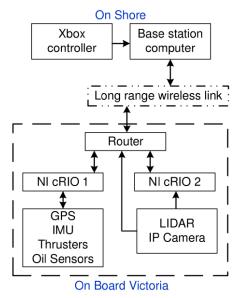
20 days of field work off Grand Isle. Search for oil spill remnants.



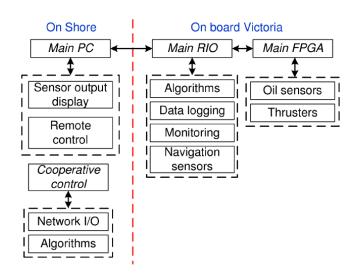
20 days of field work off Grand Isle. Search for oil spill remnants. Georgia Tech Savannah Robotics Team (led by Fumin Zhang).

(Loading Video...)

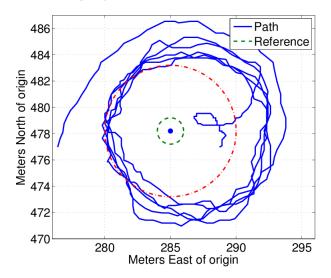
Schematic of ASV Victoria's Electrical Systems



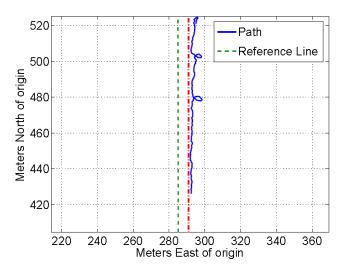
Schematic of ASV Victoria's Software Architecture



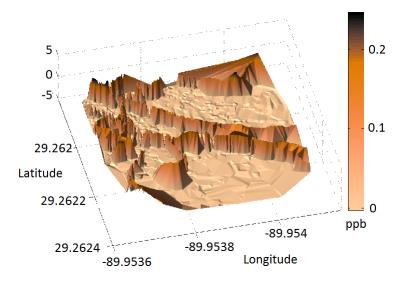
Circle Tracking by ASV Victoria



Line Tracking by ASV Victoria



Crude Oil Concentration Maps



Adaptive nonlinear controllers are useful for many engineering control systems with delays and uncertainties.

Adaptive nonlinear controllers are useful for many engineering control systems with delays and uncertainties.

Curve tracking controllers for autonomous marine vehicles are important for monitoring water quality, especially after oil spills.

Adaptive nonlinear controllers are useful for many engineering control systems with delays and uncertainties.

Curve tracking controllers for autonomous marine vehicles are important for monitoring water quality, especially after oil spills.

Our curve trackers are adaptive and robust to the perturbations and time delays that commonly arise in field work.

Adaptive nonlinear controllers are useful for many engineering control systems with delays and uncertainties.

Curve tracking controllers for autonomous marine vehicles are important for monitoring water quality, especially after oil spills.

Our curve trackers are adaptive and robust to the perturbations and time delays that commonly arise in field work.

We can prove these properties using input-to-state stability, parameter estimators, and Lyapunov-Krasovskii functionals.

Adaptive nonlinear controllers are useful for many engineering control systems with delays and uncertainties.

Curve tracking controllers for autonomous marine vehicles are important for monitoring water quality, especially after oil spills.

Our curve trackers are adaptive and robust to the perturbations and time delays that commonly arise in field work.

We can prove these properties using input-to-state stability, parameter estimators, and Lyapunov-Krasovskii functionals.

We used our controls on student built marine robots to map residual crude oil from the Deepwater Horizon spill.

Adaptive nonlinear controllers are useful for many engineering control systems with delays and uncertainties.

Curve tracking controllers for autonomous marine vehicles are important for monitoring water quality, especially after oil spills.

Our curve trackers are adaptive and robust to the perturbations and time delays that commonly arise in field work.

We can prove these properties using input-to-state stability, parameter estimators, and Lyapunov-Krasovskii functionals.

We used our controls on student built marine robots to map residual crude oil from the Deepwater Horizon spill.

In our future work, we will study adaptive robust control for heterogeneous fleets of autonomous marine vehicles.

References for 2D Case with Hyperlinks

Malisoff, M., F. Mazenc, and F. Zhang, "Stability and robustness analysis for curve tracking control using input-to-state stability," *IEEE Transactions on Automatic Control*, Volume 57, Issue 5, May 2012, pp. 1320-1326.

Malisoff, M., and F. Zhang, "Adaptive control for planar curve tracking under controller uncertainty," *Automatica*, Volume 49, Issue 5, May 2013, pp. 1411-1418

Mukhopadhyay, S., C. Wang, M. Patterson, M. Malisoff, and F. Zhang, "Collaborative autonomous surveys in marine environments affected by oil spills," in *Cooperative Robots and Sensor Networks, Second Edition*, Anis Koubaa, Ed., Studies in Computational Intelligence Series, Springer, accepted for publication in January 2014.

References for 3D Case with Hyperlinks

Malisoff, M., and F. Zhang, "Robustness of a class of three-dimensional curve tracking control laws under time delays and polygonal state constraints," in *Proceedings of the American Control Conference (Washington, DC, 17-19 June 2013)*, pp. 5710-5715.

Malisoff, M., and F. Zhang, "An adaptive control design for 3D curve tracking based on robust forward invariance," in *Proceedings of the 52nd IEEE Conference on Decision and Control (Florence, Italy, 10-13 December 2013)*, pp. 4473-4478.