Adaptive Tracking and Parameter Identification for Nonlinear Control Systems

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Specify u(t, Y) to get a singly parameterized family

$$\dot{\mathbf{Y}} = \mathcal{G}(t, \mathbf{Y}, \delta(t)), \quad \mathbf{Y} \in \mathcal{Y},$$
(2)

where  $\mathcal{G}(t, Y, d) = \mathcal{F}(t, Y, \boldsymbol{u}(t, Y), d)$ .

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Find  $\gamma_i$ 's by building certain strict LFs for  $\dot{Y} = \mathcal{G}(t, Y, 0)$ .

A LF for  $\dot{Y} = \mathcal{G}(t, Y)$  is a proper positive definite  $C^1$  function V that admits a nonnegative definite function W such that  $V_t(t, Y) + V_Y(t, Y)\mathcal{G}(t, Y) \leq -W(Y)$  for all  $t \geq 0$  and  $Y \in \mathcal{Y}$ .

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If, in addition, W is positive definite, then we call V strict.

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Warning 1: For each constant  $\bar{\delta} > 0$ , we can find a  $Y_0$  such that the solution  $\phi(t, Y_0)$  for  $\dot{Y} = -\frac{Y}{1+Y^2} + \bar{\delta}$  is unbounded.

Assume that we have a controller *u* such that

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Then

$$\dot{Y} = f(t, Y) + g(t, Y) \left[ u(t, Y) - \overline{D_x V(t, Y)} \cdot g(t, Y) + \delta \right]$$
(4)

is ISS with respect to actuator errors  $\delta$  in any control set.

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Flight control, electrical and mechanical engineering, etc. Persistent excitation. Annaswamy, Narendra, Teel.

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Our adaptive controllers have the form

$$\boldsymbol{\boldsymbol{\omega}} = \dot{\boldsymbol{\xi}}_{\boldsymbol{R}}(t) - \boldsymbol{\omega}(\boldsymbol{\xi})\hat{\boldsymbol{\Gamma}} + \boldsymbol{\mathcal{K}}(\boldsymbol{\xi}_{\boldsymbol{R}}(t) - \boldsymbol{\xi}), \quad \dot{\boldsymbol{\Gamma}} = -\boldsymbol{\omega}(\boldsymbol{\xi})^{\top}(\boldsymbol{\xi}_{\boldsymbol{R}}(t) - \boldsymbol{\xi}).$$

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Classical PE assumption:  $\exists$  constants  $T, \mu > 0$  s.t.

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Novelty: Our global strict Lyapunov function for the  $Y = (\Gamma - \hat{\Gamma}, \xi - \xi_R)$  dynamics gave ISS with respect to  $\delta$ .

We solved the tracking and identification problem for

$$\begin{cases} \dot{x} = f(\xi) \\ \dot{z}_i = g_i(\xi) + k_i(\xi) \cdot \theta_i + \psi_i \mathbf{u}_i, \quad i = 1, 2, \dots, s. \end{cases}$$
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Main PE Assumption:

We solved the tracking and identification problem for

$$\begin{cases} \dot{x} = f(\xi) \\ \dot{z}_i = g_i(\xi) + k_i(\xi) \cdot \theta_i + \psi_i \boldsymbol{u}_i, \quad i = 1, 2, \dots, s. \end{cases}$$
(9)

 $(\mathbf{x},\mathbf{z})\in\mathbb{R}^{r+s}.\ \Gamma=(\theta,\psi)=(\theta_1,...,\theta_s,\psi_1,\ldots,\psi_s)\in\mathbb{R}^{p_1+\ldots+p_s+s}.$ 

The  $C^2$  *T*-periodic reference trajectory  $\xi_R = (x_R, z_R)$  to be tracked is assumed to satisfy  $\dot{x}_R(t) = f(\xi_R(t)) \ \forall t \ge 0$ .

Main PE Assumption: positive definiteness of the matrices

$$\mathcal{P}_i \stackrel{\text{def}}{=} \int_0^T \lambda_i^\top(t) \lambda_i(t) \, \mathrm{d}t, \ 1 \le i \le s$$
 (10)

where  $\lambda_i(t) = (k_i(\xi_R(t)), \dot{z}_{R,i}(t) - g_i(\xi_R(t)))$  for each *i*.

We know v<sub>f</sub> and a global strict LF V for

$$\begin{cases} \dot{X} = f((X,Z) + \xi_R(t)) - f(\xi_R(t)) \\ \dot{Z} = v_f(t,X,Z) \end{cases}$$
(11)

such that -V and V have positive definite quadratic lower bounds near 0,

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• There are known positive constants  $\theta_M$ ,  $\psi$  and  $\overline{\psi}$  such that

$$\underline{\psi} < \psi_i < \overline{\psi} \quad \text{and} \quad |\theta_i| < \theta_M$$
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for each  $i \in \{1, 2, \dots, s\}$ .

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for each  $i \in \{1, 2, ..., s\}$ . Known directions for the  $\psi_i$ 's.

The estimator evolves on  $\{\prod_{i=1}^{s} (-\theta_M, \theta_M)^{p_i}\} \times (\psi, \overline{\psi})^s$ .

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$$\begin{cases} \dot{\hat{\theta}}_{i,j} = (\hat{\theta}_{i,j}^2 - \theta_M^2) \varpi_{i,j}, \ 1 \le i \le s, 1 \le j \le p_i \\ \dot{\hat{\psi}}_i = (\hat{\psi}_i - \underline{\psi}) (\hat{\psi}_i - \overline{\psi}) \Upsilon_i, \ 1 \le i \le s \end{cases}$$
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Here  $\hat{\theta}_i = (\hat{\theta}_{i,1}, \dots, \hat{\theta}_{i,p_i})$  for  $i = 1, 2, \dots, s$ ,

$$\varpi_{i,j} = -\frac{\partial V}{\partial \tilde{z}_{i}}(t,\tilde{\xi})k_{i,j}(\tilde{\xi}+\xi_{R}(t)) \text{ and}$$

$$\Upsilon_{i} = -\frac{\partial V}{\partial \tilde{z}_{i}}(t,\tilde{\xi})u_{i}(t,\tilde{\xi},\hat{\theta},\hat{\psi}) .$$

$$u_{i}(t,\tilde{\xi},\hat{\theta},\hat{\psi}) = \frac{v_{f,i}(t,\tilde{\xi})-g_{i}(\xi)-k_{i}(\xi)\cdot\hat{\theta}_{i}+\dot{z}_{R,i}(t)}{\hat{\psi}_{i}}$$
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$$\varpi_{i,j} = -\frac{\partial V}{\partial \tilde{z}_i} (t, \tilde{\xi}) k_{i,j} (\tilde{\xi} + \xi_R(t)) \text{ and} \\ \Upsilon_i = -\frac{\partial V}{\partial \tilde{z}_i} (t, \tilde{\xi}) u_i (t, \tilde{\xi}, \hat{\theta}, \hat{\psi}) . \\ u_i (t, \tilde{\xi}, \hat{\theta}, \hat{\psi}) = \frac{v_{t,i} (t, \tilde{\xi}) - g_i (\xi) - k_i (\xi) \cdot \hat{\theta}_i + \dot{z}_{R,i} (t)}{\hat{\psi}_i}$$
(15)

The estimator and feedback can only depend on things we know.

$$\begin{aligned}
\dot{\tilde{x}} &= f(\tilde{\xi} + \xi_{R}(t)) - f(\xi_{R}(t)) \\
\dot{\tilde{z}}_{i} &= v_{f,i}(t,\tilde{\xi}) + k_{i}(\tilde{\xi} + \xi_{R}(t)) \cdot \tilde{\theta}_{i} \\
&\quad + \tilde{\psi}_{i} u_{i}(t,\tilde{\xi},\hat{\theta},\hat{\psi}), \quad 1 \leq i \leq s \\
\dot{\tilde{\theta}}_{i,j} &= -\left(\hat{\theta}_{i,j}^{2} - \theta_{M}^{2}\right) \varpi_{i,j}, \quad 1 \leq i \leq s, \quad 1 \leq j \leq p_{i} \\
\dot{\tilde{\psi}}_{i} &= -\left(\hat{\psi}_{i} - \underline{\psi}\right) \left(\hat{\psi}_{i} - \overline{\psi}\right) \Upsilon_{i}, \quad 1 \leq i \leq s.
\end{aligned}$$
(16)

$$\begin{cases} \dot{\tilde{x}} = f(\tilde{\xi} + \xi_{R}(t)) - f(\xi_{R}(t)) \\ \dot{\tilde{z}}_{i} = v_{f,i}(t,\tilde{\xi}) + k_{i}(\tilde{\xi} + \xi_{R}(t)) \cdot \tilde{\theta}_{i} \\ + \tilde{\psi}_{i} u_{i}(t,\tilde{\xi},\hat{\theta},\hat{\psi}), \quad 1 \leq i \leq s \\ \dot{\tilde{\theta}}_{i,j} = -\left(\frac{\hat{\theta}_{i,j}^{2} - \theta_{M}^{2}}{\tilde{\psi}_{i}}\right) \varpi_{i,j}, \quad 1 \leq i \leq s, \quad 1 \leq j \leq p_{i} \\ \dot{\tilde{\psi}}_{i} = -\left(\hat{\psi}_{i} - \underline{\psi}\right) \left(\hat{\psi}_{i} - \overline{\psi}\right) \Upsilon_{i}, \quad 1 \leq i \leq s. \end{cases}$$
(16)

Tracking error:  $\tilde{\xi} = (\tilde{x}, \tilde{z}) = \xi - \xi_R = (x - x_R, z - z_R)$ Parameter estimation errors:  $\tilde{\theta}_i = \theta_i - \hat{\theta}_i$  and  $\tilde{\psi}_i = \psi_i - \hat{\psi}_i$ 

$$\begin{cases} \dot{\tilde{x}} = f(\tilde{\xi} + \xi_{R}(t)) - f(\xi_{R}(t)) \\ \dot{\tilde{z}}_{i} = v_{f,i}(t,\tilde{\xi}) + k_{i}(\tilde{\xi} + \xi_{R}(t)) \cdot \tilde{\theta}_{i} \\ + \tilde{\psi}_{i} u_{i}(t,\tilde{\xi},\hat{\theta},\hat{\psi}), \quad 1 \leq i \leq s \\ \dot{\tilde{\theta}}_{i,j} = -\left(\frac{\hat{\theta}_{i,j}^{2} - \theta_{M}^{2}}{\tilde{\psi}_{i}}\right) \varpi_{i,j}, \quad 1 \leq i \leq s, \quad 1 \leq j \leq p_{i} \\ \dot{\tilde{\psi}}_{i} = -\left(\hat{\psi}_{i} - \underline{\psi}\right) \left(\hat{\psi}_{i} - \overline{\psi}\right) \Upsilon_{i}, \quad 1 \leq i \leq s. \end{cases}$$
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$$\mathcal{Y} = \mathbb{R}^{r+s} \times \left( \prod_{i=1}^{s} \left\{ \prod_{j=1}^{p_i} (\theta_{i,j} - \theta_M, \theta_{i,j} + \theta_M) \right\} \right) \\ \times \left( \prod_{i=1}^{s} (\psi_i - \overline{\psi}, \psi_i - \underline{\psi}) \right).$$

We build a strict LF for the augmented tracking and identification vector  $Y = (\tilde{\xi}, \tilde{\theta}, \tilde{\psi}) = (\xi - \xi_R, \theta - \hat{\theta}, \psi - \hat{\psi})$  dynamics on  $\mathcal{Y}$ .

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We start with this nonstrict barrier type LF on  $\mathcal{Y}$ :

$$\begin{aligned} V_1(t,\tilde{\xi},\tilde{\theta},\tilde{\psi}) &= V(t,\tilde{\xi}) + \sum_{i=1}^s \sum_{j=1}^{p_i} \int_0^{\widetilde{\theta}_{i,j}} \frac{m}{\theta_M^2 - (m - \theta_{i,j})^2} \mathrm{d}m \\ &+ \sum_{i=1}^s \int_0^{\widetilde{\psi}_i} \frac{m}{(\psi_i - m - \underline{\psi})(\overline{\psi} - \psi_i + m)} \mathrm{d}m \,. \end{aligned}$$

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On  $\mathcal{Y}$ ,  $\dot{V}_1 \leq -W(\tilde{\xi})$  for some positive definite function W.

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We transform  $V_1$  into the desired strict LF.

# **Our Transformation**

#### **Our Transformation**

Theorem: We can construct  $K \in \mathcal{K}_{\infty} \cap C^1$  such that

$$V^{\sharp}(t,\tilde{\xi},\tilde{\theta},\tilde{\psi}) \stackrel{\text{def}}{=} \mathcal{K}\big(V_{1}(t,\tilde{\xi},\tilde{\theta},\tilde{\psi})\big) + \sum_{i=1}^{s} \overline{\Omega}_{i}(t,\tilde{\xi},\tilde{\theta},\tilde{\psi}) \quad , \qquad (17)$$

where 
$$\overline{\Omega}_{i}(t, \tilde{\xi}, \tilde{\theta}, \tilde{\psi}) = -\tilde{z}_{i}\lambda_{i}(t)\alpha_{i}(\tilde{\theta}_{i}, \tilde{\psi}_{i}) + \frac{1}{\tau\overline{\psi}}\alpha_{i}^{\top}(\tilde{\theta}_{i}, \tilde{\psi}_{i})\Omega_{i}(t)\alpha_{i}(\tilde{\theta}_{i}, \tilde{\psi}_{i})$$
, (18)

$$\alpha_{i}(\widetilde{\theta}_{i},\widetilde{\psi}_{i}) = \begin{bmatrix} \widetilde{\theta}_{i}\psi_{i} - \theta_{i}\widetilde{\psi}_{i} \\ \widetilde{\psi}_{i} \end{bmatrix}, \text{ and}$$

$$\Omega_{i}(t) = \int_{t-T}^{t} \int_{m}^{t} \lambda_{i}^{\top}(s)\lambda_{i}(s)\mathrm{d}s\mathrm{d}m ,$$
(19)

is a strict LF for the  $Y = (\tilde{\xi}, \tilde{\theta}, \tilde{\psi})$  dynamics on  $\mathcal{Y}$ .

Linear magnetic circuit.

$$\begin{cases} \dot{y}_{1} = y_{2} \\ \dot{y}_{2} = -\frac{B}{M}y_{2} - \frac{N}{M}\sin(y_{1}) + K_{\tau}[K_{b}\zeta_{1} + 1]\zeta_{2} \\ \dot{\zeta}_{i} = H_{i}(y,\zeta)\beta_{i} + \gamma_{i}\boldsymbol{u}_{i}, \quad i = 1,2 \end{cases}$$
(20)

$$\begin{cases} \dot{y}_{1} = y_{2} \\ \dot{y}_{2} = -\frac{B}{M}y_{2} - \frac{N}{M}\sin(y_{1}) + \mathcal{K}_{\tau}[\mathcal{K}_{b}\zeta_{1} + 1]\zeta_{2} \\ \dot{\zeta}_{i} = \mathcal{H}_{i}(y,\zeta)\beta_{i} + \gamma_{i}\boldsymbol{u}_{i}, \quad i = 1,2 \end{cases}$$

$$\mathcal{H}_{1}(y,\zeta) = (-\zeta_{1}, y_{2}\zeta_{2}).$$
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$$H_{1}(y,\zeta) = (-\zeta_{1}, y_{2}\zeta_{2}). \quad H_{2}(y,\zeta) = (-\zeta_{2}, -y_{2}\zeta_{1}, -y_{2}).$$
(20)

Linear magnetic circuit. Drives single-link, direct-drive robot arm.

$$\begin{cases} \dot{y}_{1} = y_{2} \\ \dot{y}_{2} = -\frac{B}{M}y_{2} - \frac{N}{M}\sin(y_{1}) + K_{\tau}[K_{b}\zeta_{1} + 1]\zeta_{2} \\ \dot{\zeta}_{i} = H_{i}(y,\zeta)\beta_{i} + \gamma_{i}u_{i}, \quad i = 1,2 \end{cases}$$
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 $H_1(y,\zeta) = (-\zeta_1, y_2\zeta_2).$   $H_2(y,\zeta) = (-\zeta_2, -y_2\zeta_1, -y_2).$ 

•  $y_1, y_2 =$  load position and velocity.

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•  $y_1, y_2 =$  load position and velocity.  $\zeta_i =$  winding currents.

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• B = viscous friction coefficient.

$$\begin{cases} \dot{y}_{1} = y_{2} \\ \dot{y}_{2} = -\frac{B}{M}y_{2} - \frac{N}{M}\sin(y_{1}) + K_{\tau}[K_{b}\zeta_{1} + 1]\zeta_{2} \\ \dot{\zeta}_{i} = H_{i}(y,\zeta)\beta_{i} + \gamma_{i}u_{i}, \quad i = 1,2 \end{cases}$$
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- $y_1, y_2 =$  load position and velocity.  $\zeta_i =$  winding currents.
- B = viscous friction coefficient. M = mechanical inertia.

$$\begin{cases} \dot{y}_{1} = y_{2} \\ \dot{y}_{2} = -\frac{B}{M}y_{2} - \frac{N}{M}\sin(y_{1}) + K_{\tau}[K_{b}\zeta_{1} + 1]\zeta_{2} \\ \dot{\zeta}_{i} = H_{i}(y,\zeta)\beta_{i} + \gamma_{i}u_{i}, \quad i = 1,2 \end{cases}$$
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- $y_1, y_2 =$ load position and velocity.  $\zeta_i =$  winding currents.
- B = viscous friction coefficient. M = mechanical inertia. N = related to the load mass and gravitational constant.  $K_{\tau}, K_{b} =$  torque transmission coefficients.
- The unknown vectors β<sub>1</sub> ∈ ℝ<sup>2</sup> and β<sub>2</sub> ∈ ℝ<sup>3</sup> and unknown scalars γ<sub>1</sub> and γ<sub>2</sub> are the motor electric parameters.





20 days of field work off Grand Isle.



20 days of field work off Grand Isle. Search for oil spill remnants.

$$\begin{cases} \dot{\rho} = -\sin(\phi) \\ \dot{\phi} = \frac{\kappa\cos(\phi)}{1+\kappa\rho} - \frac{u_2}{2}, \quad (\rho,\phi) \in (0,+\infty) \times (-\pi/2,\pi/2) \end{cases}$$
(21)

$$\begin{cases} \dot{\rho} = -\sin(\phi) \\ \dot{\phi} = \frac{\kappa\cos(\phi)}{1+\kappa\rho} - U_2, \quad (\rho,\phi) \in (0,+\infty) \times (-\pi/2,\pi/2) \end{cases}$$
(21)

$$\frac{\mathbf{u}_{2}}{\mathbf{u}_{2}} = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi)$$
(22)

$$\begin{cases} \dot{\rho} = -\sin(\phi) \\ \dot{\phi} = \frac{\kappa\cos(\phi)}{1+\kappa\rho} - \frac{u_2}{2}, \quad (\rho,\phi) \in (0,+\infty) \times (-\pi/2,\pi/2) \end{cases}$$
(21)

$$U_{2} = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi)$$
(22)

$$h(\rho) = \alpha \left\{ \rho + \frac{\rho_0^2}{\rho} - 2\rho_0 \right\}$$
(23)
# **Curve Tracking Dynamics**

$$\begin{cases} \dot{\rho} = -\sin(\phi) \\ \dot{\phi} = \frac{\kappa\cos(\phi)}{1+\kappa\rho} - \frac{u_2}{2}, \quad (\rho,\phi) \in (0,+\infty) \times (-\pi/2,\pi/2) \end{cases}$$
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$$U_2 = \frac{\kappa \cos(\phi)}{1 + \kappa \rho} - h'(\rho) \cos(\phi) + \mu \sin(\phi)$$
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$$U_{2}(\rho,\phi) = -h'(\rho)\sin(\phi) + \frac{1}{\mu}\int_{0}^{V(\rho,\phi)}\Gamma_{0}(m)\mathrm{d}m$$
 (25)

We can use  $U_2$  to prove ISS of the perturbed closed loop system

$$\dot{\rho} = -\sin(\phi), \quad \dot{\phi} = h'(\rho)\cos(\phi) - \mu\sin(\phi) + \delta$$
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with respect to  $\delta : [0, \infty) \to [-\delta_*, \delta_*]$  on forward invariant sets.

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# Adaptive Robust Curve Tracking

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$$\begin{cases} \dot{\rho} = -\sin(\phi) \\ \dot{\phi} = \frac{\kappa\cos(\phi)}{1+\kappa\rho} - K_2[\mathbf{v}+\delta] \end{cases}$$
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### Adaptive Robust Curve Tracking

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(27)

We proved ISS of the tracking and identification dynamics

$$\begin{cases} \dot{\tilde{q}}_{1} = -\sin(\tilde{q}_{2}) \\ \dot{\tilde{q}}_{2} = \frac{\kappa\cos(\tilde{q}_{2})}{1+\kappa(\tilde{q}_{1}+\rho_{0})} - \frac{K_{2}}{\tilde{K}_{2}+K_{2}} \boldsymbol{u}_{2} - K_{2}\delta \\ \dot{\tilde{K}}_{2} = -(\tilde{K}_{2}+K_{2}-\boldsymbol{c}_{\min})(\boldsymbol{c}_{\max}-\tilde{K}_{2}-K_{2})\frac{\partial U_{2}}{\partial \phi} \frac{\boldsymbol{u}_{2}}{\tilde{K}_{2}+K_{2}} \end{cases}$$
(28)

for  $(\tilde{q}_1, \tilde{q}_2, \tilde{K}_2) = (\rho - \rho_0, \phi, \hat{K}_2 - K_2)$  on each set in a nested sequence of sets that fill the state space.

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- Our strict Lyapunov function approach gave key robustness properties such as input-to-state stability.
- We aim to find extensions that apply under time delays and state constraints including obstacle avoidance.