# Adaptive Tracking and Parameter Identification for Nonlinear Control Systems 

Michael Malisoff, Louisiana State University Sponsored by AFOSR, NSF/DMS, and NSF/ECCS

Department of Mathematical Sciences Talk
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Specify $u(t, Y)$ to get a singly parameterized family

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\begin{equation*}
\dot{Y}=\mathcal{G}(t, Y, \delta(t)), \quad Y \in \mathcal{Y}, \tag{2}
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where $\mathcal{G}(t, Y, d)=\mathcal{F}(t, Y, u(t, Y), d)$.

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Find $\gamma_{i}$ 's by building certain strict LFs for $\dot{Y}=\mathcal{G}(t, Y, 0)$.

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Warning 1: For each constant $\bar{\delta}>0$, we can find a $Y_{0}$ such that the solution $\phi\left(t, Y_{0}\right)$ for $\dot{Y}=-\frac{Y}{1+Y^{2}}+\bar{\delta}$ is unbounded.

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\begin{equation*}
\dot{Y}=f(t, Y)+g(t, Y)[u(t, Y)-\overbrace{D_{X} V(t, Y) \cdot g(t, Y)}^{L_{g} V(t, Y)}+\delta] \tag{4}
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is ISS with respect to actuator errors $\delta$ in any control set.

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## Adaptive Tracking and Parameter Identification

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Classical PE assumption: $\exists$ constants $T, \mu>0$ s.t.

$$
\begin{equation*}
\mu \operatorname{Id}_{p \times p} \leq \int_{t-T}^{t} \omega\left(\xi_{R}(I)\right)^{\top} \omega\left(\xi_{R}(I)\right) \mathrm{d} / \quad \text { for all } t \in \mathbb{R} . \tag{8}
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Our adaptive controllers have the form

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u=\dot{\xi}_{R}(t)-\omega(\xi) \hat{\Gamma}+K\left(\xi_{R}(t)-\xi\right), \quad \dot{\hat{\Gamma}}=-\omega(\xi)^{\top}\left(\xi_{R}(t)-\xi\right)
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Classical PE assumption: $\exists$ constants $T, \mu>0$ s.t.

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\begin{equation*}
\mu \operatorname{Id}_{p \times p} \leq \int_{t-T}^{t} \omega\left(\xi_{R}(I)\right)^{\top} \omega\left(\xi_{R}(I)\right) \mathrm{d} / \quad \text { for all } t \in \mathbb{R} . \tag{8}
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Novelty:

## First-Order (Mazenc, de Queiroz, M., '09)

In 2009, we gave a solution for the special case

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Novelty: Our global strict Lyapunov function for the $Y=\left(\Gamma-\hat{\Gamma}, \xi-\xi_{R}\right)$ dynamics gave ISS with respect to $\delta$.

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We solved the tracking and identification problem for

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\dot{x}=f(\xi)  \tag{9}\\
\dot{z}_{i}=g_{i}(\xi)+k_{i}(\xi) \cdot \theta_{i}+\psi_{i} u_{i}, \quad i=1,2, \ldots, s .
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Main PE Assumption: positive definiteness of the matrices

$$
\begin{equation*}
\mathcal{P}_{i} \stackrel{\text { def }}{=} \int_{0}^{T} \lambda_{i}^{\top}(t) \lambda_{i}(t) \mathrm{d} t, \quad 1 \leq i \leq s \tag{10}
\end{equation*}
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where $\lambda_{i}(t)=\left(k_{i}\left(\xi_{R}(t)\right), \dot{z}_{R, i}(t)-g_{i}\left(\xi_{R}(t)\right)\right)$ for each $i$.

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- We know $v_{f}$ and a global strict LF $V$ for

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The estimator evolves on $\left\{\prod_{i=1}^{s}\left(-\theta_{M}, \theta_{M}\right)^{p_{i}}\right\} \times(\underline{\psi}, \bar{\psi})^{s}$.

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The estimator and feedback can only depend on things we know.

## Augmented Error Dynamics

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\left\{\begin{align*}
\dot{\tilde{x}}= & f\left(\tilde{\xi}+\xi_{R}(t)\right)-f\left(\xi_{R}(t)\right)  \tag{16}\\
\dot{\tilde{z}}_{i}= & v_{f, i}(t, \tilde{\xi})+k_{i}\left(\tilde{\xi}+\xi_{R}(t)\right) \cdot \tilde{\theta}_{i} \\
& +\widetilde{\psi}_{i} u_{i}(t, \tilde{\xi}, \hat{\theta}, \hat{\psi}), 1 \leq i \leq s \\
\dot{\tilde{\theta}}_{i, j}= & -\left(\hat{\theta}_{i, j}^{2}-\theta_{M}^{2}\right) \varpi_{i, j}, 1 \leq i \leq s, 1 \leq j \leq p_{i} \\
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Tracking error: $\tilde{\xi}=(\tilde{x}, \tilde{z})=\xi-\xi_{R}=\left(x-x_{R}, z-z_{R}\right)$ Parameter estimation errors: $\widetilde{\theta}_{i}=\theta_{i}-\hat{\theta}_{i}$ and $\widetilde{\psi}_{i}=\psi_{i}-\hat{\psi}_{i}$

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Parameter estimation errors: $\widetilde{\theta}_{i}=\theta_{i}-\hat{\theta}_{i}$ and $\widetilde{\psi}_{i}=\psi_{i}-\hat{\psi}_{i}$

$$
\begin{aligned}
\mathcal{Y}= & \mathbb{R}^{r+s} \times\left(\prod_{i=1}^{s}\left\{\prod_{j=1}^{p_{i}}\left(\theta_{i, j}-\theta_{M}, \theta_{i, j}+\theta_{M}\right)\right\}\right) \\
& \times\left(\prod_{i=1}^{s}\left(\psi_{i}-\bar{\psi}, \psi_{i}-\underline{\psi}\right)\right) .
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## Stabilization Analysis

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We build a strict LF for the augmented tracking and identification vector $Y=(\tilde{\xi}, \tilde{\theta}, \tilde{\psi})=\left(\xi-\xi_{R}, \theta-\hat{\theta}, \psi-\hat{\psi}\right)$ dynamics on $\mathcal{Y}$.

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We start with this nonstrict barrier type LF on $\mathcal{Y}$ :

$$
\begin{aligned}
V_{1}(t, \tilde{\xi}, \tilde{\theta}, \tilde{\psi})= & V(t, \tilde{\xi})+\sum_{i=1}^{s} \sum_{j=1}^{p_{i}} \int_{0}^{\tilde{\theta}_{i, j}} \frac{m}{\theta_{M}^{2}-\left(m-\theta_{i, j}\right)^{2}} \mathrm{~d} m \\
& +\sum_{i=1}^{s} \int_{0}^{\widetilde{\psi}_{i}} \frac{m}{\left(\psi_{i}-m-\underline{\psi}\right)\left(\bar{\psi}-\psi_{i}+m\right)} \mathrm{d} m .
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We transform $V_{1}$ into the desired strict LF.

## Our Transformation

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Theorem: We can construct $K \in \mathcal{K}_{\infty} \cap C^{1}$ such that

$$
\begin{align*}
& V \sharp(t, \tilde{\xi}, \tilde{\theta}, \tilde{\psi}) \stackrel{\text { def }}{=} K\left(V_{1}(t, \tilde{\xi}, \tilde{\theta}, \tilde{\psi})\right)+\sum_{i=1}^{s} \bar{\Omega}_{i}(t, \tilde{\xi}, \tilde{\theta}, \widetilde{\psi}),  \tag{17}\\
& \text { where } \quad \bar{\Omega}_{i}(t, \tilde{\xi}, \tilde{\theta}, \tilde{\psi})=-\tilde{z}_{i} \lambda_{i}(t) \alpha_{i}\left(\widetilde{\theta}_{i}, \widetilde{\psi}_{i}\right) \\
&+\frac{1}{T \bar{\psi}} \alpha_{i}^{\top}\left(\widetilde{\theta}_{i}, \widetilde{\psi}_{i}\right) \Omega_{i}(t) \alpha_{i}\left(\widetilde{\theta}_{i}, \widetilde{\psi}_{i}\right),  \tag{18}\\
& \alpha_{i}\left(\widetilde{\theta}_{i}, \widetilde{\psi}_{i}\right)= {\left[\begin{array}{c}
\tilde{\theta}_{i} \psi_{i}-\theta_{i} \tilde{\psi}_{i} \\
\widetilde{\psi}_{i}
\end{array}\right], \text { and } }  \tag{19}\\
& \Omega_{i}(t)= \int_{t-T}^{t} \int_{m}^{t} \lambda_{i}^{\top}(s) \lambda_{i}(s) \mathrm{d} s \mathrm{~d} m
\end{align*}
$$

is a strict LF for the $Y=(\tilde{\xi}, \tilde{\theta}, \tilde{\psi})$ dynamics on $\mathcal{Y}$.

## Application: BLDC Motor (Dawson-Hu-Burg)

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Linear magnetic circuit.

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\left\{\begin{array}{l}
\dot{y}_{1}=y_{2}  \tag{20}\\
\dot{y}_{2}=-\frac{B}{M} y_{2}-\frac{N}{M} \sin \left(y_{1}\right)+K_{\tau}\left[K_{b} \zeta_{1}+1\right] \zeta_{2} \\
\dot{\zeta}_{i}=H_{i}(y, \zeta) \beta_{i}+\gamma_{i} u_{i}, \quad i=1,2
\end{array}\right.
$$

## Application: BLDC Motor (Dawson-Hu-Burg)

Linear magnetic circuit. Drives single-link, direct-drive robot arm.

$$
\begin{align*}
& \left\{\begin{aligned}
\dot{y}_{1} & =y_{2} \\
\dot{y}_{2} & =-\frac{B}{M} y_{2}-\frac{N}{M} \sin \left(y_{1}\right)+K_{\tau}\left[K_{b} \zeta_{1}+1\right] \zeta_{2} \\
\dot{\zeta}_{i} & =H_{i}(y, \zeta) \beta_{i}+\gamma_{i} u_{i}, \quad i=1,2
\end{aligned}\right.  \tag{20}\\
& H_{1}(y, \zeta)
\end{align*}=\left(-\zeta_{1}, y_{2} \zeta_{2}\right) . .
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- $y_{1}, y_{2}=$ load position and velocity.


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\end{align*}
$$

- $y_{1}, y_{2}=$ load position and velocity. $\zeta_{i}=$ winding currents.
- $B=$ viscous friction coefficient. $M=$ mechanical inertia. $N=$ related to the load mass and gravitational constant. $K_{\tau}, K_{b}=$ torque transmission coefficients.
- The unknown vectors $\beta_{1} \in \mathbb{R}^{2}$ and $\beta_{2} \in \mathbb{R}^{3}$ and unknown scalars $\gamma_{1}$ and $\gamma_{2}$ are the motor electric parameters.


## Application: Marine Robots (with Georgia Tech)

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20 days of field work off Grand Isle.

## Application: Marine Robots (with Georgia Tech)



20 days of field work off Grand Isle. Search for oil spill remnants.

## Curve Tracking Dynamics

## Curve Tracking Dynamics

$$
\left\{\begin{align*}
\dot{\rho} & =-\sin (\phi)  \tag{21}\\
\dot{\phi} & =\frac{\kappa \cos (\phi)}{1+\kappa \rho}-u_{2}, \quad(\rho, \phi) \in(0,+\infty) \times(-\pi / 2, \pi / 2)
\end{align*}\right.
$$

## Curve Tracking Dynamics

$$
\begin{align*}
& \left\{\begin{array}{l}
\dot{\rho}=-\sin (\phi) \\
\dot{\phi}=\frac{k \cos (\phi)}{1+\kappa \rho}-u_{2}, \quad(\rho, \phi) \in(0,+\infty) \times(-\pi / 2, \pi / 2)
\end{array}\right.  \tag{21}\\
& u_{2}=\frac{\kappa \cos (\phi)}{1+\kappa \rho}-h^{\prime}(\rho) \cos (\phi)+\mu \sin (\phi) \tag{22}
\end{align*}
$$

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\end{array}\right.  \tag{21}\\
& u_{2}=\frac{\kappa \cos (\phi)}{1+\kappa \rho}-h^{\prime}(\rho) \cos (\phi)+\mu \sin (\phi)  \tag{22}\\
& h(\rho)=\alpha\left\{\rho+\frac{\rho_{0}^{2}}{\rho}-2 \rho_{0}\right\} \tag{23}
\end{align*}
$$

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\left\{\begin{array}{c}
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u_{2}=\frac{\kappa \cos (\phi)}{1+\kappa \rho}-h^{\prime}(\rho) \cos (\phi)+\mu \sin (\phi) \\
h(\rho)=\alpha\left\{\rho+\frac{\rho_{0}^{2}}{\rho}-2 \rho_{0}\right\}  \tag{24}\\
V(\rho, \phi)=-\ln (\cos (\phi))+h(\rho)
\end{array}\right.
$$

## Curve Tracking Dynamics

$$
\begin{gather*}
\left\{\begin{array}{l}
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h(\rho)=\alpha\left\{\rho+\frac{\rho_{0}^{2}}{\rho}-2 \rho_{0}\right\} \\
V(\rho, \phi)=-\ln (\cos (\phi))+h(\rho) \\
U_{2}(\rho, \phi)=-h^{\prime}(\rho) \sin (\phi)+\frac{1}{\mu} \int_{0}^{v(\rho, \phi)} \Gamma_{0}(m) \mathrm{d} m
\end{array}, .\right. \tag{21}
\end{gather*}
$$

## Robustly Forwardly Invariant Hexagons

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We can use $U_{2}$ to prove ISS of the perturbed closed loop system

$$
\begin{equation*}
\dot{\rho}=-\sin (\phi), \quad \dot{\phi}=h^{\prime}(\rho) \cos (\phi)-\mu \sin (\phi)+\delta \tag{26}
\end{equation*}
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with respect to $\delta:[0, \infty) \rightarrow\left[-\delta_{*}, \delta_{*}\right]$ on forward invariant sets.

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$$
\begin{aligned}
& A=\left(\rho_{*}, 0\right), B=\left(2 \rho_{*}, \mu \rho_{*}\right), \\
& C=\left(\rho_{*}+K \rho_{o}, \mu \rho_{*}\right), D=\left(\rho_{*}+K \rho_{o}, 0\right), \\
& E=\left(K \rho_{o},-\mu \rho_{*}\right), F=\left(\rho_{*},-\mu \rho_{*}\right), \\
& \mu \tan \left(\mu \rho_{*}\right)>\left\|h^{\prime}\right\|_{\left[\rho_{*}, \rho_{*}+K \rho_{0}\right]}
\end{aligned}
$$

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\end{aligned}
$$

$$
\left.\mu \tan \left(\mu \rho_{*}\right)>\left\|h^{\prime}\right\|_{\left[\rho_{*}, \rho_{*}\right.}+K \rho_{0}\right]
$$

Tight Disturbance Bound:

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& \mu \tan \left(\mu \rho_{*}\right)>\left\|h^{\prime}\right\|_{\left[\rho_{*}, \rho_{*}+K \rho_{0}\right]}
\end{aligned}
$$

Tight Disturbance Bound: Choose any $\delta_{*} \in\left(0, \min \left\{\Delta_{*}, \Delta_{* *}\right\}\right)$.

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& \mu \tan \left(\mu \rho_{*}\right)>\left\|h^{\prime}\right\|\left[\rho_{*}, \rho_{*}+K \rho_{0}\right]
\end{aligned}
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Tight Disturbance Bound: Choose any $\delta_{*} \in\left(0, \min \left\{\Delta_{*}, \Delta_{* *}\right\}\right)$.
$\Delta_{*}=\min \left\{\left|h^{\prime}(\rho) \cos (\phi)\right|:(\rho, \phi)^{\top} \in \mathrm{AB} \cup \mathrm{ED}\right\}$
$\Delta_{* *}=\min \left\{\left|h^{\prime}(\rho) \cos (\phi)-\mu \sin (\phi)\right|:(\rho, \phi)^{\top} \in \mathrm{BC} \cup E F\right\}$.

## Adaptive Robust Curve Tracking

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$$
\left\{\begin{array}{l}
\dot{\rho}=-\sin (\phi)  \tag{27}\\
\dot{\phi}=\frac{\kappa \cos (\phi)}{1+\kappa \rho}-K_{2}[v+\delta]
\end{array}\right.
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$$
\left\{\begin{array}{l}
\dot{\rho}=-\sin (\phi)  \tag{27}\\
\dot{\phi}=\frac{\kappa \cos (\phi)}{1+\kappa \rho}-K_{2}[v+\delta]
\end{array}\right.
$$

We proved ISS of the tracking and identification dynamics

$$
\left\{\begin{array}{l}
\dot{\tilde{q}}_{1}=-\sin \left(\tilde{q}_{2}\right)  \tag{28}\\
\dot{\tilde{q}}_{2}=\frac{\kappa \cos \left(\tilde{( }_{2}\right)}{1+\kappa\left(\tilde{( }_{1}+\rho_{0}\right)}-\frac{K_{2}}{\dot{K}_{2}+K_{2}} u_{2}-K_{2} \delta \\
\dot{\tilde{K}}_{2}=-\left(\tilde{K}_{2}+K_{2}-c_{\min }\right)\left(c_{\max }-\tilde{K}_{2}-K_{2}\right) \frac{\partial U_{2}}{\partial \phi} \frac{u_{2}}{\dot{K}_{2}+K_{2}}
\end{array}\right.
$$

for $\left(\tilde{q}_{1}, \tilde{q}_{2}, \tilde{K}_{2}\right)=\left(\rho-\rho_{0}, \phi, \hat{K}_{2}-K_{2}\right)$ on each set in a nested sequence of sets that fill the state space.

Conclusions

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- Nonlinear control systems are ubiquitous in aerospace, bio, electrical, and mechanical engineering.


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- Our strict Lyapunov function approach gave key robustness properties such as input-to-state stability.


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- One central problem is to build functions called closed loop controllers that force desired tracking behaviors.
- We designed controllers for several applications including models with unknown parameters that we can identify.
- Our strict Lyapunov function approach gave key robustness properties such as input-to-state stability.
- We aim to find extensions that apply under time delays and state constraints including obstacle avoidance.

